Structure Type Study

BRIDGE NO. FRA-CO376-0327 WINCHESTER PIKE OVER BLACKLICK CREEK

December, 2013



Prepared by:



Prepared for: Franklin County Engineer's Office 970 Dublin Road Columbus, Ohio 43215

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I. INTRODUCTION

This report addresses the development of the preferred bridge alternative for Bridge No. FRA-CO376-0327, Winchester Pike over Blacklick Creek for the County of Franklin.

The existing bridge is a three-span, continuous steel beam structure with a reinforced concrete deck (non-composite) on cap-and-column piers and stub abutments with spill-through slopes. Each substructure includes 12" diameter cast-in-place reinforced concrete piles. The bridge was constructed in 1954 and rehabilitated in 1992. The bridge is located in the Southeast Franklin County and Canal Winchester region. In recent years, the Blacklick Creek Greenway Trail was constructed underneath the bridge adjacent to the east abutment.

Two options for widening the existing structure to accommodate a turning lane were presented in the initial Scope of Work: a Low Speed Design and a High Speed Design. A meeting on February 28, 2013 with the Franklin County Engineer's resulted in selection of the High-Speed Design option, which provides for wider lanes and shoulders. Further, asymmetrical versus symmetrical widening was considered the most cost-effective for this option due to fewer impacts to the trail way, no additional right-of-way impacts, and fewer pier columns in the creek. The High-Speed option will utilize widening on the north side only.

The general appraisal on the most recent bridge inspection report indicates the existing structure is in very good condition. Therefore, widening will be performed utilizing the existing superstructure and substructures to their fullest extent with no rehabilitation to these units anticipated. Additional work includes widening the existing approach slabs and any necessary for the sustained use of the trail way.

The Structure Type Study follows Section 201.2 of the ODOT Bridge Design Manual. A preliminary site plan, transverse section, typical abutment section, preliminary phase construction details, narrative of bridge work, cost estimate, and foundation recommendations are presented. The Hydraulic Report, Geotechnical Exploration Report and Preliminary Maintenance of Traffic Plan are contained under separate cover.

II. DESIGN CONSIDERATIONS

The FRA-CO376-0327 Bridge spans Blacklick Creek, which is a waterway with a defined floodplain and floodway. The proposed widening with new pier columns added in the creek will not result in a post-project rise in the base flood profile for Blacklick Creek. This is further addressed in the Hydraulic Report.

In the cross frame bay between the existing north exterior beam and adjacent interior beam are nine 3½" diameter AT&T telephone ducts. These ducts also pass through each abutment



backwall and under the approach slabs. The lines are likely to contain asbestos and are to remain in service with no disturbance during construction.

As per ODOT BDM Section 304.3.3, the new railing at the widening is to be Twin Steel Tube Bridge Railing as per ODOT Standard TST-1-99. This railing has an acceptance level equal to NCHRP Test Level 4 (TL-4). The minimum acceptable level is TL-3. The existing railing on the opposite side of the bridge, where no widening is proposed, is Deep Beam Bridge Guardrail as per ODOT Standard DBR-2-73. The NCHRP test level for this railing is TL-2. To accommodate TL-3, this existing DBR-2-73 guardrail will require replacement with new TST-1-99 railing or be upgraded to DBR-3-11, Deep Beam Bridge Retrofit Railing. To compliment the new TST-1-99 railing at the widening, it is recommended to replace the existing railing with TST-1-99. This would require removing a portion of the existing deck overhang to construct a new overhang to attach the new railing. As a cost savings, Franklin County may suggest retrofitting with the DBR-3-11.

III. NARRATIVE OF PROPOSED BRIDGE WORK

Per the Scope of Work, additional structure types, such as concrete, were not considered. The most practical solution would be to widen the existing structure with a reinforced concrete deck non-composite with steel beams, on widened substructures.

Preliminary analysis indicates that the new superstructure widening could be accomplished utilizing one new beam line. A 4'-0" maximum deck overhang, per BDM recommendations, was used to minimize the new 10'-4" beam spacing. During deck pour, the bottom flange will require bracing at some locations to eliminate potential beam warping due to the dead load on the large overhang. Consideration was given to using two lighter beams with a smaller beam spacing and overhang, to eliminate the need for bracing during the deck pour. A comparative cost analysis (not included) was performed to justify using the one beam option. Results showed that using two beams would be \$24,350 more. This included quantity differences between steel, concrete, painting, bearings and additional bracing. Because of this cost savings, it is recommended to use the one beam option, and for this reason, only one alternative is presented.

The widened bridge will accommodate three (3) lanes of traffic: one in each direction and one turning lane. The existing horizontal and vertical alignment is to be maintained as close as possible.

The design method for the widened alternative follows the AASHTO LFD Specifications and the 2004 ODOT Bridge Design Manual. The design loading is HS20-44 for both the Superstructure and Substructures. The design loading includes Case II and the Alternate Military Loading with a 60 P.S.F. future wearing surface.



Two phases will be incorporated into construction of the widening. Traffic will first be shifted to the south side of the bridge deck to accommodate construction of the north widening. Then traffic will be shifted to the newly constructed north side to allow the replacement of the south edge of the deck and installment of the new railing. Sheet piling left-in-place will be used at the approaches behind the abutment backwall during construction of the widening. The portion of the Greenway Trail under the bridge will most likely be closed during construction.

The following provides information regarding specific design considerations. Preliminary Structure Site Plan and Profile, Typical Sections and Phase Construction Details can be found in the Preliminary Bridge Details Section (Section V).

Foundation Recommendations

The subsurface investigation for this project site consisted of 16 test borings made between July 8 and July 15, 2013, to accommodate widening existing abutments and piers. Four borings were investigated for the proposed bridge widening, one at each substructure unit. Existing fill materials were encountered at each boring location ranging from 7.5 to 18 feet deep. Underlying the existing fill materials, the borings encountered natural, primarily cohesive soils. Bedrock was not encountered. Laboratory tests were performed to determine soil classification and engineering characteristics.

Based on the information provided in the Geotechnical Exploration Report, we recommend the proposed widening of the existing abutment substructures be supported on 12" cast-in-place concrete friction-type piles. The proposed widening of the existing pier substructures are recommended to be supported on 14" cast-in-place concrete friction-type piles. Four piles are suggested for each abutment and four piles for each pier.

The estimated lengths rounded to the nearest 5 feet for the Rear Abutment are 50 feet and 60 feet for the Forward Abutment. The estimated length rounded to the nearest 5 feet for each pier is 45 feet.

Proposed Structure (Widening)

• Reference Chord and Skew: The existing bridge was constructed on a tangent alignment utilizing the existing reference chord, which is a line between the intersections of the existing abutment bearings and existing Beam 3. The proposed widening will be constructed with this same reference chord. The proposed skew of 30°-00'-00" Left Forward, which is the same as existing, is measured to the reference chord.



- Alignment: In the vicinity of the bridge, a new 0°-48'-13" right curve alignment is defined along the centerline of construction of Winchester Pike to closely match the geometry of the existing 0°-48' right curve alignment. The stationing of the centerline of bearings of the substructures is along the centerline of construction of Winchester Pike. The original alignment of the centerline of construction intersected the reference chord at the centerline of the existing abutment bearings. The new alignment places the proposed centerline of construction slightly to the south and consequently results in variable shoulder widths across the bridge.
- Foundation Type: The proposed foundation for the widened abutments consists of 12" diameter cast-in-place concrete piling similar to existing. The proposed foundation for the widened piers consists of 14" diameter cast-in-place concrete piling. As a result of preliminary analysis, it is anticipated that four piles will be required for each abutment widening and four piles for each pier footing cap.
- Substructure Type: The existing abutment widening is proposed to be similar to the existing abutment section, which is a stub abutment cap type with a backwall. The existing piers are proposed to be widened using new caps connected to the existing columns and adding one new square column to each.
- Approach Slabs: The existing full-width approach slabs will be widened to their new full-width requirement. The length will match the existing length of 20'-0".
- Bridge Spans: The spans will remain the same: 48'-0", 60'-0", 48'-0". These spans are measured center-to-center of bearings along the reference chord.
- Bridge Width: The bridge width is comprised of (3) 12'-0" lanes and variable shoulder widths on each side for a total of 52'-1" face-to-face of rails.
- Framing Layout: The new beam shall be ASTM A709 Grade 50W (weathering steel), which complements the existing A588 50 ksi beams. The new beam size will be W36 x 150, which has very similar section properties as the existing W36 x 135. The need for a heavier beam is due to wider proposed spacing and larger overhang.

The Average Daily Truck Traffic (ADTT) is well below 2500, which places the bridge in a Case II Fatigue category. Although Type 1 intermediate cross frames are typically used for Case II bridges, modified Type 3 are proposed. Top and bottom chords with single erection bolts will be used for stability during the deck pour. Once the deck has cured, the top chords will be removed and diagonals will be added. Both the diagonals and bottom chords will be field welded at this time.

• Bearings: The proposed bearings shall be elastomeric with internal laminates similar to the existing.



- Superstructure Type: The proposed superstructure widening will consist of a concrete deck non-composite (to match existing) with the new beam. The proposed deck thickness is 9 inches. Since the new railing type is Twin Steel Tube Bridge Railing, over-the-side drainage will require a steel drip strip. The existing deck ends utilize a structural expansion joint with an elastomeric strip seal. It is proposed to extend the joint with the same type using Item 516, Horizontal Extension of Structural Expansion Joint.
- Painting: Each end of the new weathering steel beam line will be shop painted for the first ten feet. Shop painting is used to eliminate containment during field painting operations.

Estimated Structure Construction Costs

The following table summarizes the initial construction cost for the bridge widening without any contingencies. Contingencies are included with the C1 estimate that is included with the AER. The construction costs below are derived from a detailed cost estimate that can be found in the Structure Construction Cost Estimate (Section IV) portion of this report. The cost estimate utilized estimated quantities and unit costs that were obtained from the ODOT Office of Estimating and the "Estimator" Program.

CONSTRUCTION COST ESTIMATE

Bridge No.	Alternative No.	Description	Initial Construction Cost
FRA-CO376-0327	Alternative 1	Widen existing deck, abutments, and piers.	\$405,725

Conclusion and Recommendation

The information in this report focuses on verifying the recommended alternative as outlined in the Scope of Services. After evaluating the information in this study, it is recommended that the **FRA-CO376-0327 Bridge** be constructed with a widened concrete deck and a new A709 Grade 50W (weathering steel) beam on widened abutments and piers.



IV. STRUCTURE CONSTRUCTION COST ESTIMATE



ALTERNATIVE 1 - COST ESTIMATE STRUCTURE TYPE STUDY Deck Widening								
ITEM	ITEM EXT.	DESCRIPTION	QTY	UNIT	UNIT PRICE	TOTAL		
202	11203	Item 202 - Portions of Structure Removed, over 20 Foot Span, as per plan	LUMP			\$12,000		
503	11100	Item 503, Cofferdams and Excavation Bracing	LUMP			\$5,000		
503	21100	Item 503 - Unclassified Excavation	60	C.Y.	\$35.00	\$2,101		
504	11101	Item 504 - Steel Sheet Piling Left in Place, as per plan	1200	S.F.	\$30.00	\$36,000		
505	11100	Item 505 - Pile Driving Equipment Mobilization	LUMP			\$10,000		
507	00500	Item 507 - 12" Cast-In-Place Reinforced Concrete Piles, Driven	440	FT.	\$12.00	\$5,280		
507	00550	Item 507 - 12" Cast-In-Place Reinforced Concrete Piles, Furnished	480	FT.	\$25.00	\$12,000		
507	00600	Item 507 - 14" Cast-In-Place Reinforced Concrete Piles, Furnished	400	FT.	\$15.00	\$6,000		
507	00650	Item 507 - 14" Cast-In-Place Reinforced Concrete Piles, Driven	360	FT.	\$30.00	\$10,800		
509	10000	Item 509 - Epoxy Coated Reinforcing Steel	29024	POUND	\$0.90	\$26,122		
509	20001	Item 509 - Reinforcing Steel, Replacement of Existing Reinforcing Steel, as per plan	100	POUND	\$2.50	\$250		
510	10000	Item 510 - Dowel Holes with nonshrink, nonmetallic grout	24	EACH	\$15.00	\$360		
511	34444	Item 511 - Class QC2 Concrete, Bridge Deck	91	C.Y.	\$675.00	\$61,531		
511	41010	Item 511 - Class QC1 Concrete, Pier Above Footings	15	C.Y.	\$550.00	\$8,511		
511	43510	Item 511 - Class QC1 Concrete, Abutment including Footing	40	C.Y.	\$480.00	\$19,137		
511	46510	Item 511 - Class QC1 Concrete, Footings	14	C.Y.	\$375.00	\$5,333		
512	10100	Item 512 - Sealing of Concrete Surfaces (Epoxy-Urethane)	329	S.Y.	\$15.00	\$4,935		
512	33000	Item 512 - Type 2 Waterproofing	13	S.Y.	\$27.00	\$360		
512	74000	Item 512 - Removal of Existing Coatings from Concrete Surfaces	185	S.Y.	\$8.35	\$1,548		
513	10260	Item 513 - Structural Steel Members, Level 3	26900	POUND	\$1.40	\$37,660		
514	80020	Item Special - Shop Painting and Field Touch-up of Structural Steel	328	S.F.	\$7.50	\$2,462		
516	11900	Item 516 - Horizontal Extension of Structural Expansion Joint	32	FT.	\$600.00	\$19,440		
516	44000	Item 516 - Elastomeric Bearing w/Internal Laminates & Load Plate (Neoprene)	4	EACH	\$800.00	\$3,200		
518	21200	Item 518 - Porous Backfill with Filter Fabric	12	C.Y.	\$65.00	\$780		
518	40000	Item 518 - 6" Perforated C.P.P.	40	FT.	\$8.00	\$320		
518	40010	Item 518 - 6" Non-Perforated C.P.P., INCLUDING SPECIALS	16	FT.	\$12.00	\$192		
526	15000	Item 526 - Reinforced Concrete Approach Slabs (T=13")	62	S.Y.	\$225.00	\$13,950		
601	32204	Item 601 - Rock Channel Protection, Type C with Fabric Filter	60	C.Y.	\$65.00	\$3,900		

TOTAL INITIAL COST W/O CONTINGENCY = \$309,171

PDP CONTINGENCY =

SUB-TOTAL COST = \$340,088

INFL CONTINGENCY = 19.30%

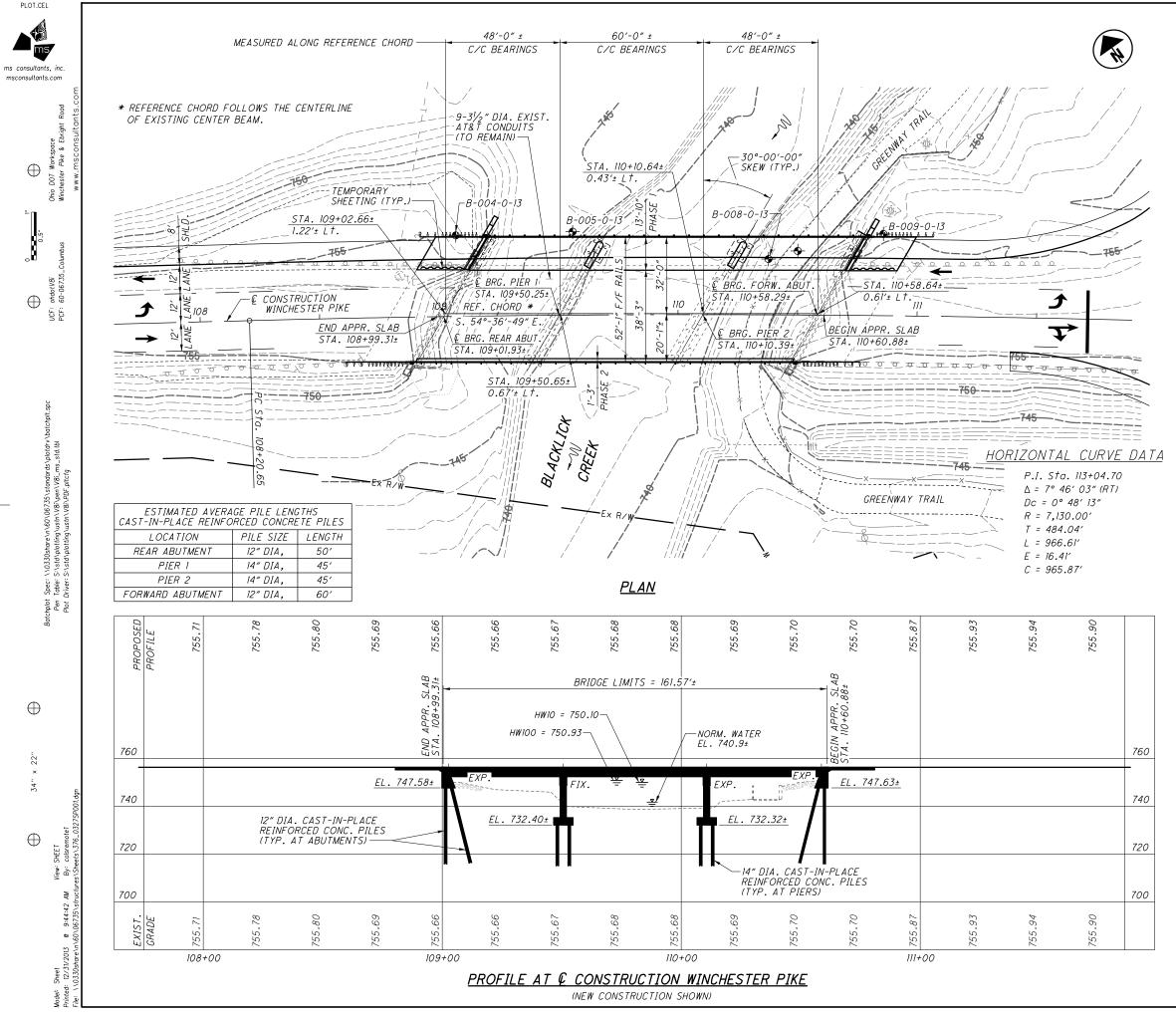
TOTAL COST = \$405,725

10.00%

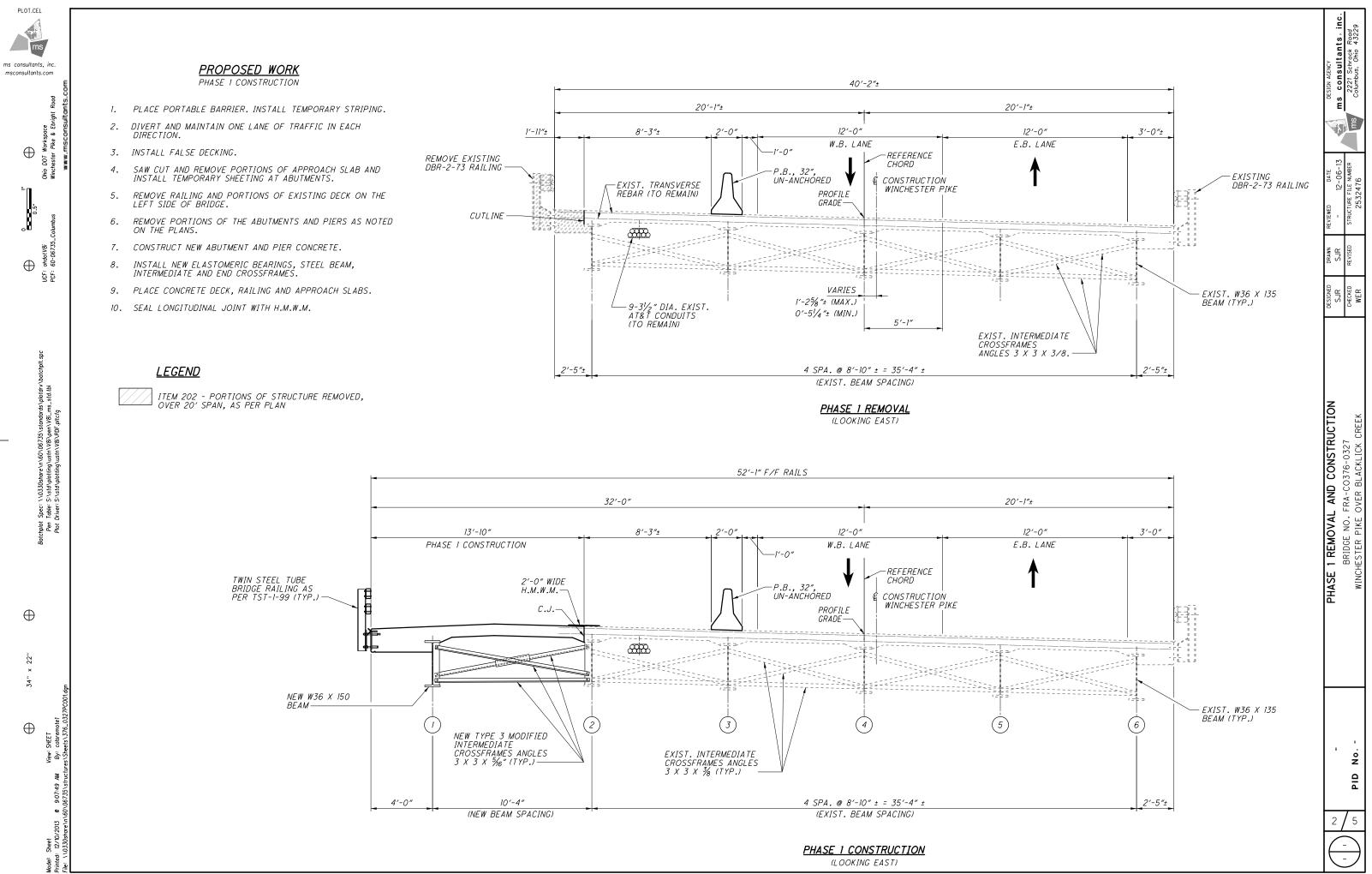


V. PRELIMINARY BRIDGE DETAILS





BENCHMARK DATA	inc.			
BM #1:	ants ; io 433			
BM #2:	DESIGN AGENCY s consultant 2221 Schrock F Columbus, Ohio 4			
FOR ADDITIONAL BENCHMARK INFORMATION. SEE ROADWAY PLAN	ms col			
NOTES	E			
EARTHWORK LIMITS SHOWN ARE APPROXIMATE. ACTUAL SLOPES SHALL CONFORM TO PLAN CROSS SECTIONS.	ate 06-13 NUMBER 76			
<u>LEGEND</u>	DATE 12-06-1 FILE NUMBI 32476			
+ BORING LOCATION	μω			
DESIGN TRAFFIC:	REVIEWED - STRUCTURE 25:			
2015 ADT = 2015 ADTT = 2025 ADTT = 2025	S] RE			
2035 ADT = 21,000 2035 ADTT = 208 DIRECTIONAL DISTRIBUTION = 0.52	DRAWN SJR REVISED			
HYDRAULIC DATA	RE			
DRAINAGE AREA = 57.4 SO. MILES Q (100) = 8700 CFS HW (100) = 750.93 V (100) = 5.73 FT/S Q (10) = 7250 CFS HW (10) = 750.10 V (10) = 5.53 FT/S STRUCTURE CLEARS THE 10 YEAR DESIGN HW BY 2.07 FEET.	DESIGNED SJR CHECKED			
EXISTING STRUCTURE	JNTY 31± 88±			
TYPE: THREE SPAN CONTINUOUS NON-COMPOSITE STEEL BEAM WITH REINFORCED CONCRETE DECK ON STUB ABUTMENTS AND CAP AND COLUMN PIERS	FRANKLIN COUNT STA.108+99.31± STA.110+60.88±			
SPANS: 48'-0"±, 60'-0"±, 48-0"± c/c BEARINGS ALONG REFERENCE CHORD	FRA ST, ST,			
ROADWAY: 40'-2" FACE TO FACE OF RAILS				
LOADING: HS20-44 CASE II AND ALTERNATE MILITARY LOADING				
SKEW: 30°-00'-00" LF TO REFERENCE CHORD				
APPROACH SLABS: AS-1-81 (20' LONG)	CREE			
ALIGNMENT: 0°-48'-00" CURVE RT.				
SUPERELEVATION: 0.026	6-032 KLICK			
STRUCTURAL FILE NUMBER: 2532476 DATE BUILT: 1954 REHABILITATED: 1992				
DISPOSITION: TO BE WIDENED	PLA A-CO: ER BL			
	E PLAN FRA-CO3 OVER BLA			
PROPOSED STRUCTURE				
PROPOSED WIDEN EXISTING CONCRETE DECK NON-COMPOSITE WORK: WITH NEW STEEL BEAM, WIDEN ABUTMENTS ON NEW CONCRETE PILES, ADD NEW PIER FOOTINGS ON CONCRETE PILES FOR NEW WIDENED CAP AND COLUMN PIERS, NEW ELASTOMERIC BEARINGS, SEAL SUB- STRUCTURES AND WIDEN APPROACH SLABS TYPE: THREE SPAN CONTINUOUS STEEL BEAM, ASTM A709 GR. 50W (NEW BEAM) AND A588 (EXISTING BEAMS), NON- COMPOSITE WITH REINFORCED CONCRETE DECK ON	SIT BRIDGE NO. WINCHESTER PIKE			
WIDENED ABUTMENTS AND CAP AND COLUMN PIERS SPANS: 48'-0"±, 60'-0"±, 48-0"± c/c BEARINGS ALONG REFERENCE				
CHORD				
ROADWAY: 52'-1" FACE TO FACE OF RAILS LOADING: HS2O-44 CASE II AND ALTERNATE MILITARY LOADING FWS = 60 PSF	י י אס ע			
SKEW: 30°-00'-00" LF TO REFERENCE CHORD				
APPROACH SLABS: AS-1-81 (20' LONG)				
ALIGNMENT: 0°-48'-13" CURVE RT.	1.7-			
SUPERELEVATION: 0.026	1/5			
COORDINATES: LATITUDE N. 39°-53′-26″ LONGITUDE W. 82°-51′-49″				
	onsultants, inc.			



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PLOT.CEL

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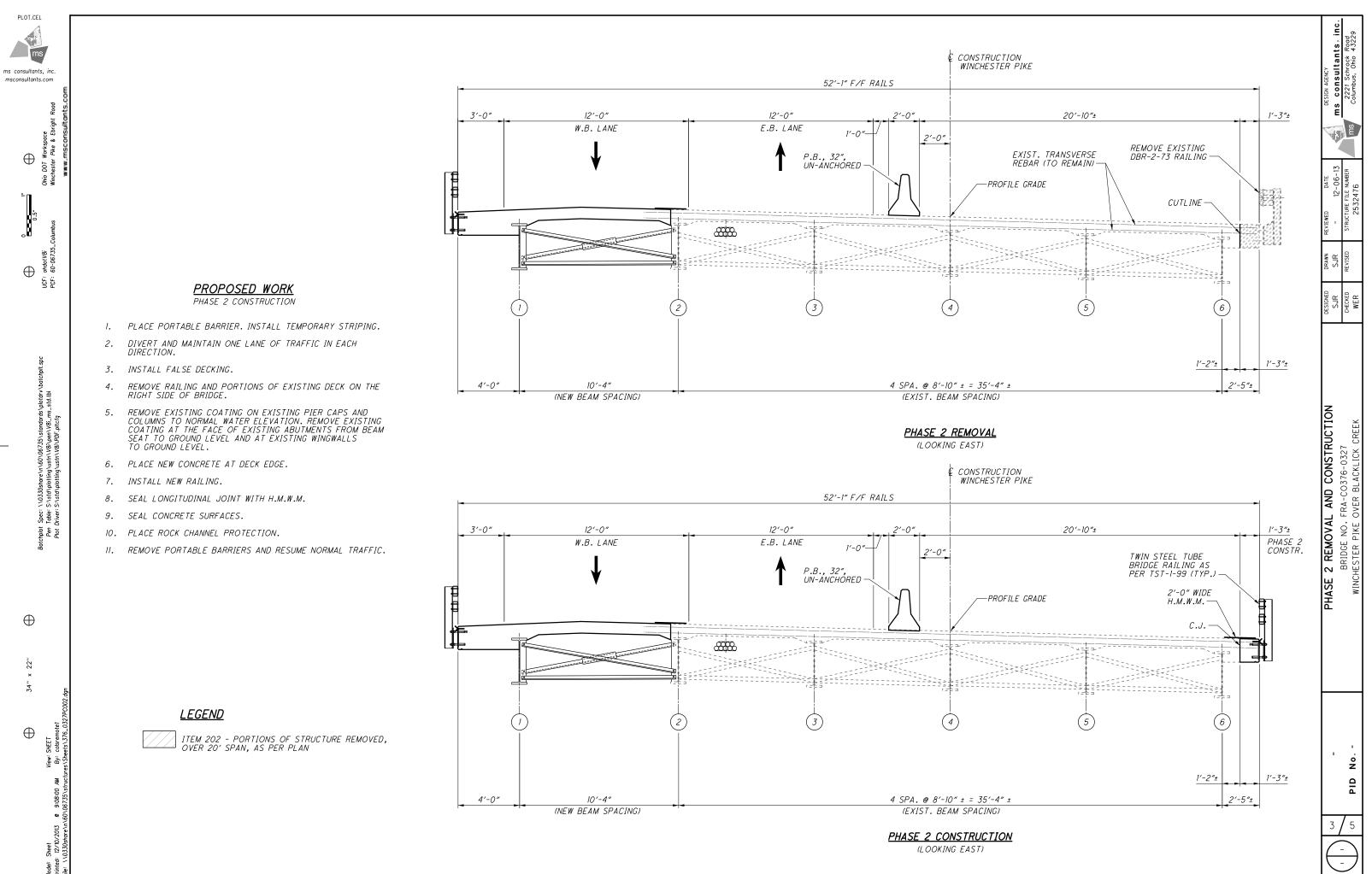
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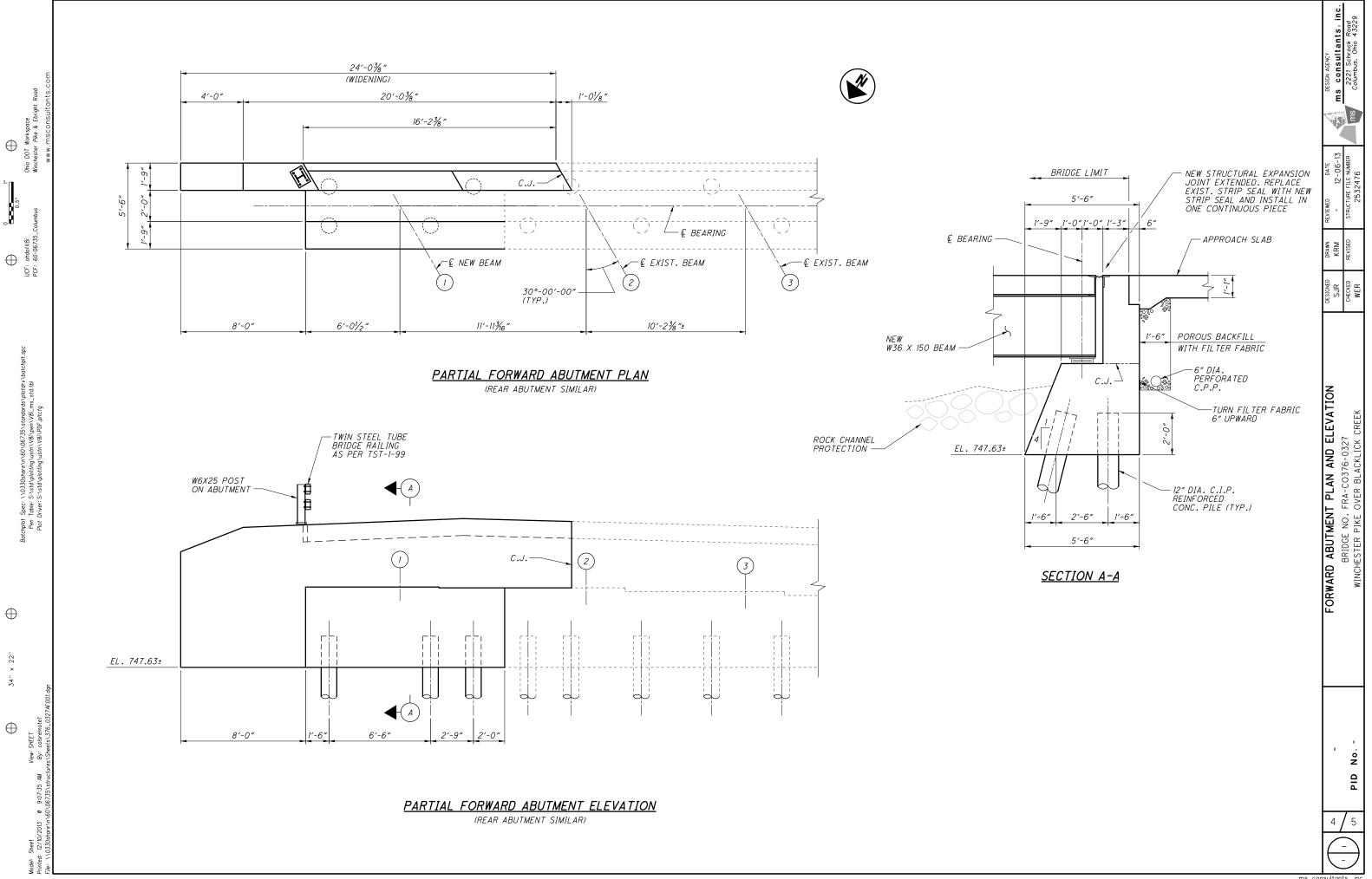
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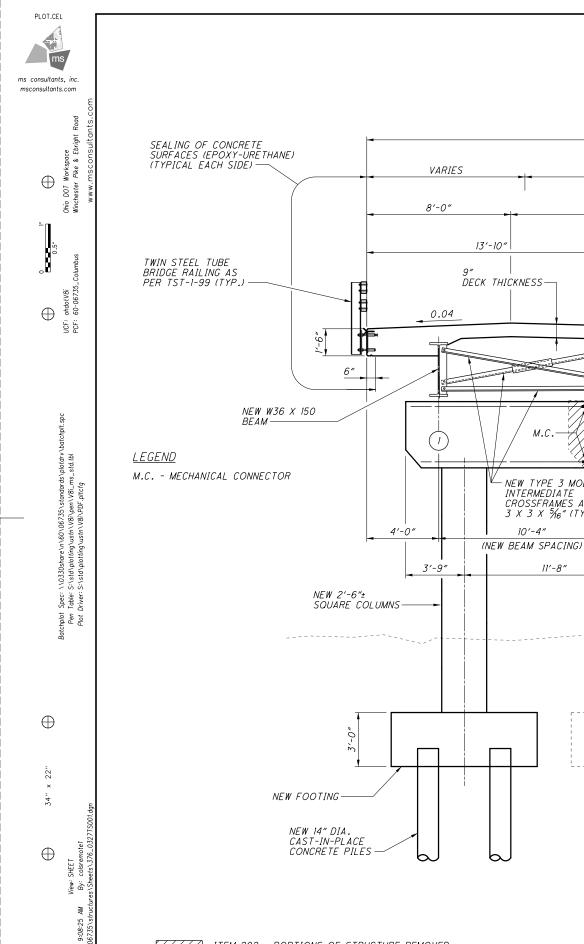
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PROPOSED TRANSVERSE SECTION AT PIER (LOOKING EAST)

K2...

52'-1" F/F RAILS

12'-0"

LANE

REFERENCE CHORD ——

PROFILE GRADE —

0.026±

12'-0"

LANE

CONSTRUCTION WINCHESTER PIKE

1'-25/8"± (MAX.)

0'-5¼"± (MIN.)

VARIES

4

4 SPA. @ 8'-10" ± = 35'-4" ±

(EXIST. BEAM SPACING)

<u>ح</u>

K3...

NORMAL WATER

EL. 740.9±-

20'-1" ±

18'-10" ±

5

EXIST. STREAM BED-

KC.

12'-0"

LANE

6″±

2

KC.,

M.C

10'-4"

- NEW TYPE 3 MODIFIED INTERMEDIATE CROSSFRAMES ANGLES 3 X 3 X 56" (TYP.)

11'-8″

-2'-0" WIDE H.M.W.M.

- 2000 C

-C.J.

3'-1"±--=

24'-0"

EXIST. INTERMEDIATE CROSSFRAMES ANGLES 3 X 3 X 3 (TYP.)-----

EXIST. REBAR TO REMAIN

KC.

18'-2" ±

-9-3½″ DIA. EXIST. AT&T CONDUITS (TO REMAIN)

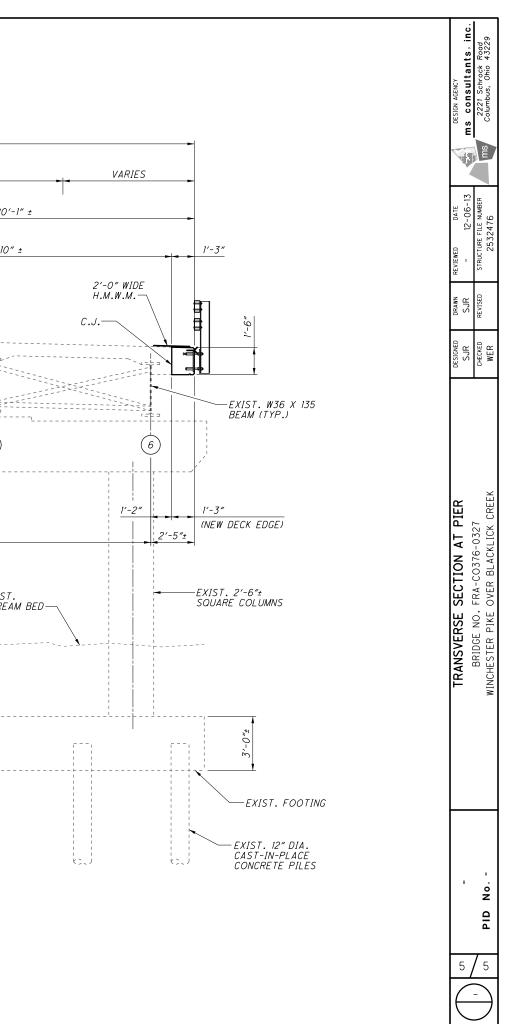
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ITEM 202 - PORTIONS OF STRUCTURE REMOVED, OVER 20' SPAN, AS PER PLAN

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Sheet 12/10/2013

NOTE: FOOTINGS AND PILES ARE NOT SHOWN AS SKEWED.



ms consultants