REPORT

OF

SUBSURFACE EXPLORATION

FOR

BIXBY ROAD, EAST ALTERNATIVE A

FRANKLIN COUNTY PID NO. 82404



Franklin County Engineer 970 Dublin Road Columbus, Ohio 43215-1169



DLZ Job No. 1121-1010.00

February 16, 2011

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REPORT OF SUBSURFACE EXPLORATION FOR BIXBY ROAD, EAST ALTERNATIVE A FRANKLIN COUNTY PID NO. 82404

1.0 INTRODUCTION

This report presents the findings of a subsurface exploration performed for the proposed roadway realignment and improvements referred to as the Bixby Road "East Alternative A", Franklin County PID No. 82404. "East Alternative A" includes the realignment of Bixby Road and Brice Road at Winchester Pike to create a new four legged intersection. This design will eliminate the existing skewed and offset intersections that currently exist at the site. The purpose of this subsurface exploration was to provide conclusions and recommendations regarding soil related design and construction considerations, pavement and subgrade recommendations, and earthwork operations. These recommendations will include CBR values for the pavement design, compaction requirements for site fill, construction backfill, and fill used to support pavements.

The geotechnical engineer has planned and supervised the performance of the geotechnical engineering services, has considered the findings, and has presented this report in accordance with generally accepted geotechnical engineering practices. No other warranties, either expressed or implied, are made as to the professional advice included in this report.

2.0 FIELD EXPLORATION

The field exploration consisted of drilling eleven borings (B-1 through B-11). In addition, nine pavement cores (C-1 through C-9) were also taken to assess existing pavement thicknesses. Borings in existing roadways were drilled using a truck-mounted, rotary drilling rig. Off road borings were drilled using an ATV-mounted rotary drilling rig. The borings were advanced using a 3-inch OD flight auger with samples collected using a 2-inch OD split spoon sampler. Pavement cores were collected using an electric diamond tipped core drill.

The soil borings and pavement cores were drilled on October 31, 2011 and January 5, 2012. All soil borings were advanced to depths of between 10 and 10.5 feet with the exception of boring B-4, which was drilled to a depth of 15.5 feet. The borings were backfilled and patched upon completion. Information concerning the drilling procedures and logs of the borings are presented in the Appendix.

The boring locations were marked in the field by a representative of DLZ Ohio, Inc. A Boring Location Plan is presented in the Appendix.

3.0 FINDINGS

3.1 Generalized Geology

The site has been glaciated by both the Wisconsin and Illinoian Glacial events. The area is reported as consisting primarily of deep glacial till with intermittent sand and gravel outwash seams.

3.2 Subsurface Conditions

This section presents the generalized descriptions of the subsurface conditions encountered by the borings. For more detailed information obtained during the subsurface investigation, please refer to the Boring Location Plan and the boring logs in the Appendix.

Topsoil was present in borings B-1, B-2, B-6, B-8, B-10, and B-11, and varied from 1 to 6 inches in thickness. Three inches of gravel was present at the surface in boring B-9. Fill or possible fill was encountered in four borings. In boring B-1, the fill consisted of stiff sandy silt (A-4a) from a depth of 0.2 to 1.5 feet. In boring B-6 the fill consisted of very stiff silty clay (A-6b) was present from a depth of 0.5 to 1.5 feet then silt and clay (A-6a) fill was encountered to a depth of 4.5 feet. Loose gravel (A-1-a) fill was encountered in boring B-8 to a depth of 1.5 feet. Possible fill consisting of very stiff brown sandy silt (A-4a) was encountered in boring B-9 from a depth of 0.3 to 1.5 feet.

Directly below the surface materials and any fill or possible fill, the natural soils generally consisted of medium stiff to hard sandy silt (A-4a), silty clay (A-6b), silt and clay (A-6a), and clay (A-7-6). Granular soils consisting of gravel (A-1-a), gravel with sand (A-1-b), fine sand (A-3), and coarse and fine sand (A-3a) were typically encountered below 6 feet below ground surface. Soft, wet silt (A-4b) was encountered in boring B-4 between the depths of 4.8 and 6.3 feet. Organic materials were encountered in the upper soils of borings B-2, B-4, and B-8. It should be noted that one sample from boring B-2 (between the depths of 0.3 and 1.5 feet) was classified as organic clay by air dried verses oven dried liquid limit analysis.

It should be expected that variations in conditions may occur between borings. Thickness and sequential relations of soil layers, composition, density, moisture, water seepage and water conditions may vary both in vertical interval and in short lateral distances. Stratification lines as indicated on the boring logs represent approximate depths of changes in texture, color, and moisture; in places the transition may be gradual and not sharply defined by a readily obvious line of demarcation.

3.3 Groundwater Conditions

In general, seepage was first encountered in several of the borings at a depth of approximately 8 feet below ground surface. Three borings had a measurable water level in the borehole at the completion of drilling. These borings were B-4 (at a depth of 13.8 feet), B-5 (at a depth of 6.7 feet), and B-7 (at a depth of 6.5 feet). It should be noted that moist and wet cohesive soils may not produce water over a short period of time. Therefore,

water levels may not be present at the completion of the drilling activities, but when an open excavation is left open for a longer period of time, water seepage may occur.

3.4 Pavement Cores

Nine pavement cores were collected to assess the thickness of pavement at select locations. The locations of the nine pavement cores are presented on the Boring Location Plan. Table 1 details the pavement materials encountered at each boring location.

Boring	Surface Asphalt (inches)	Brick (inches)	Concrete (inches)	Aggregate (inches)
C-1	16			
C-2	9.5	3.5	6	
C-3	5.5			
C-4	6			6
C-5	9		10	
C-6	9	3.5	6.5	
C-7	2		8.5	
C-8	9			8
C-9	7			8

 Table 1. Pavement Materials

3.5 Laboratory Testing

In the laboratory, soil samples were examined and visually classified by an engineering geologist. The moisture content, grain size distribution, and Atterberg limits were determined for representative samples obtained from the borings. Laboratory test results are presented in the Appendix and summaries are included on the boring logs.

4.0 ANALYSES AND RECOMMENDATIONS

4.1 General

The subgrade soils encountered in the borings are generally considered acceptable as subgrade materials. However, some of the subgrade soils had moisture contents exceeding their optimum moisture contents and many had N-values below 10, indicating soft or loose materials. Soils containing elevated organic content were encountered in three borings, but only one sample was classified as organic lean clay (A-8b) by laboratory testing. Organic soils should be anticipated in other areas during construction.

The soils encountered near the proposed subgrade levels for the project were analyzed for suitability in accordance with the Ohio Department of Transportation, Office of Geotechnical Engineering document, "Geotechnical Bulletin 1: Plan Subgrades (GB-1)," issued July 15, 2010. The results of these analyses can be found in the Appendix. The near-surface subgrade soils encountered by the borings were generally very similar across the site. Consequently, all of the borings were used to calculate a design CBR of 6.

Generally, subgrade soils with a moisture content exceeding the optimum moisture content of the soil by three or more percentage points, have low N-values, or that were classified as silt are considered to be problematic soils. The results of the borings indicate that most of the subgrade soils exceed the optimum moisture content or have low N-values. The results of the analyses indicated some type of subgrade treatment will likely be needed for all of the new construction and the subgrades below existing roadways.

Once the existing pavements and unsuitable materials are removed to achieve the required subgrade elevation and prior to the placement of ODOT Item 304 aggregate base, the entire subgrade should be proofrolled in accordance with the Ohio Department of Transportation (ODOT) Construction Materials Specifications (CMS) 204.06. A geotechnical engineer or engineering geologist should be present to observe the proofrolling operations and to identify areas of organic or unsuitable soils. If unsuitable or organic soils are observed during proofrolling, the material should be removed and replaced with suitable compacted material. Alternatively, unsuitable soils that are soft and wet may be scarified or disced, dried to within $\pm 3\%$ of the optimum moisture content (as required to achieve stability), and recompacted in accordance with ASTM D698.

If the project is to be constructed using the 2010 ODOT Construction and Material Specifications (CMS), the top twelve inches below the subgrade level and 18 inches beyond the edge of the surface of the pavement must be prepared in accordance with ODOT item 204.03. If satisfactory subgrade stability cannot be obtained, areas of unsuitable soils should be undercut to a depth of 18 inches below subgrade elevation and replaced with compacted Type B or Type C granular material (ODOT CMS Item 703.16.C).

Soils classified as silt (A-4b) were identified during the subsurface exploration. Per ODOT CMS 203.03A, silt is not permitted as an embankment material within the top 3 feet below the surface of the subgrade.

All subgrades should be graded to drain to an underdrain, catch basin, pipe, or ditch. The subgrade should then be compacted and proofrolled in accordance with ODOT CMS Item 204.03, "Compaction of Subgrade" and Item 204.06, "Proof Rolling."

5.0 CLOSING REMARKS

The conclusions and recommendations presented in this report are based on information disclosed by a limited number of borings widely spaced throughout the project area. The boring information must be extrapolated to determine the subsurface conditions occurring along the entire alignment. This extrapolation is based on the knowledge of soil and rock forming geologic processes and on past experience. Therefore, the recommendations presented in this report are based in part on the assumption that certain natural conditions will actually be encountered and not altered during construction. Consequently, it is recommended that construction monitoring and testing be performed to establish that soil conditions at the site are as assumed.

This subsurface investigation was performed based solely upon a geotechnical standpoint. No environmental site assessment or testing was performed as part of the exploration.

We appreciate being given the opportunity to be of service to you on this project. Please do not hesitate to call if we may be of further assistance or you have any questions concerning the exploration or the recommendations presented in this report.

Sincerely,

DLZ OHIO, INC.

Brian E. Mott, P.G. Sr. Geologist

Timothy A. Hampshire, MSCE, P.E. Geotechnical Engineering Division Manager

APPENDIX

General Information Drilling Procedures and Logs of Borings Legend – Boring Log Terminology Boring Location Plan Boring Logs – 11 Borings Pavement Core Logs – 9 Core Holes Laboratory Test Results Ohio Department of Transportation (ODOT) GB-1 Subgrade Analyses Results

GENERAL INFORMATION DRILLING PROCEDURES AND LOGS OF BORINGS

Drilling and sampling were conducted in accordance with procedures generally recognized and accepted as standardized methods of investigation of subsurface conditions concerning geotechnical engineering considerations. Borings were drilled with either a truck-mounted or ATV-mounted drill rig.

Drive split-barrel sampling was performed in 1.5 foot increments at intervals not exceeding 5 feet. In the event the sampler encountered resistance to penetration of 6 inches or less after 50 blows of the drop hammer, the sampling increment was discontinued. Standard penetration data were recorded and one or more representative samples were preserved from each sampling increment.

In borings where rock was cored, NXM or NQ size diamond coring tools were used.

In the laboratory all samples were visually classified by a geotechnical engineer. Moisture contents of representative fine-grained soil samples were determined. A limited number of samples, considered representative of foundation materials present, were selected for performance of grain-size analyses and plasticity characteristics tests. The results of these tests are shown on the boring logs.

The boring logs included in the Appendix have been prepared on the basis of the field record of drilling and sampling, and the results of the laboratory examination and testing of samples. Stratification lines on the boring logs indicating changes in soil stratigraphy represent depths of changes approximated by the driller, by sampling effort and recovery, and by laboratory test results. Actual depths to changes may differ somewhat from the estimated depths, or transitions may occur gradually and not be sharply defined. The boring logs presented in this report therefore contain both factual and interpretative information and are not an exact copy of the field log.

Although it is considered that the borings have disclosed information generally representative of site conditions, it should be expected that between borings conditions may occur which are not precisely represented by any one of the borings. Soil deposition processes and natural geologic forces are such that soil and rock types and conditions may change in short vertical intervals and horizontal distances.

Soil/rock samples will be stored at our laboratory for a period of six months. After this period of time, they will be discarded, unless notified to the contrary by the client.

LEGEND – BORING LOG TERMINOLOGY

Explanation of each column, progressing from left to right

- 1. Depth (in feet) refers to distance below the ground surface.
- 2. Elevation (in feet) is referenced to mean sea level, unless otherwise noted.
- 3. Standard Penetration (N) the number of blows required to drive a 2-inch O.D., 1-3/8 inch I.D., split-barrel sampler, using a 140-pound hammer with a 30-inch free fall. The blows are recorded in 6-inch drive increments. Standard penetration resistance is determined from the total number of blows required for one foot of penetration by summing the second and third 6-inch increments of an 18-inch drive.

50/n – indicates number of blows (50) to drive a split-barrel sampler a certain number of inches (n) other than the normal 6-inch increment.

- 4. The length of the sampler drive is indicated graphically by horizontal lines across the "Standard Penetration" and "Recovery" columns.
- 5. Sample recovery from each drive is indicated numerically in the column headed "Recovery".
- 6. The drive sample location is designated by the heavy vertical bar in the "Sample No., Drive" column.
- 7. The length of hydraulically pressed "Undisturbed" samples is indicated graphically by horizontal lines across the "Press" column.
- 8. Sample numbers are designated consecutively, increasing in depth.
- 9. Soil Description
 - a. The following terms are used to describe the relative compactness and consistency of soils:

Granular Soils – Compactness

	Blows/Foot
<u>Term</u>	Standard Penetration
Very Loose	0-4
Loose	4 - 10
Medium Dense	10 – 30
Dense	30 – 50
Verv Dense	over 50

Cohesive Soils - Consistency

	Unconfined	Blows/Foot	
	Compression	Standard	
Term	tons/sq.ft.	Penetration	Hand Manipulation
Very Soft	less than 0.25	below 2	Easily penetrated by fist
Soft	0.25 – 0.50	2 – 4	Easily penetrated by thumb
Medium Stiff	0.50 – 1.0	4 – 8	Penetrated by thumb with moderate pressure
Stiff	1.0 – 2.0	8 – 15	Readily indented by thumb but not penetrated
Very Stiff	2.0 - 4.0	15 – 30	Readily indented by thumb nail
Hard	over 4.0	over 30	Indented with difficulty by thumb nail

- b. Color If a soil is a uniform color throughout, the term is single, modified by such adjective as light and dark. If the predominant color is shaded by a secondary color, the secondary color precedes the primary color. If two major and distinct colors are swirled throughout the soil, the colors are modified by the term "mottled".
- c. Texture is based on the Ohio Department of Transportation Classification System. Soil particle size definitions are as follows:

Description	Size	Description	<u>Size</u>					
Boulders	Larger than 8"	Sand – Coarse	2.0 mm to 0.42 mm					
Cobbles	8" to 3"	– Fine	0.42 mm to 0.074 mm					
Gravel – Coarse	3" to ³ ⁄4"	Silt	0.074 mm to 0.005 mm					
– Fine	³ ⁄4" to 2.0 mm	Clay	smaller than 0.005 mm					

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- d. The main soil component is listed first. The minor components are listed in order of decreasing percentage of particle size.
- e. Modifiers to main soil descriptions are indicated as a percentage by weight of particle sizes.

trace	0 to 10%
little	10 to 20%
some	20 to 35%
"and"	35 to 50%

f. Moisture content of **cohesionless soils** (sands and gravels) is described as follows:

<u>Term</u>	Relative Moisture or Appearance
Dry	No moisture present
Damp	Internal moisture, but none to little surface moisture
Moist	Free water on surface
Wet	Voids filled with free water

g. The moisture content of cohesive soils (silts and clays) is expressed relative to plastic properties.

<u>Term</u>	Relative Moisture or Appearance
Dry	Powdery
Damp	Moisture content slightly below plastic limit
Moist	Moisture content above plastic limit but below liquid limit
Wet	Moisture content above liquid limit

10. Rock Hardness and Rock Quality Designation

a. The following terms are used to describe the relative strength of the **bedrock**.

Term Description Very Weak Core can be carved with a knife and scratched by fingernail. Can be excavated readily with a point of a pick. Pieces 1-inch or more in thickness can be broken by finger pressure. Weak Core can be grooved or gouged readily by a knife or pick. Can be excavated in small fragments by moderate blows of a pick point. Small, thin pieces can be broken by finger pressure. Slightly Strong Core can be grooved or gouged 0.05 inch deep by firm pressure of a knife or pick point. Can be excavated in small chips to pieces about 1-inch maximum size by hard blows of the point of a geologist's pick. Core can be scratched with a knife or pick. Grooves or gouges to ¹/₄" deep can be Moderately Strong excavated by hand blows of a geologist's pick. Requires moderate hammer blows to detach hand specimen. Strong Core can be scratched with a knife or pick only with difficulty. Requires hard hammer blows to detach hand specimen. Sharp and resistant edges are present on hand specimen. Core cannot be scratched by a knife or sharp pick. Breaking of hand specimens requires Very Strong hard repeated blows of the geologist hammer. Extremely Strong Core cannot be scratched by a knife or sharp pick. Chipping of hand specimens requires hard repeated blows of the geologist hammer.

- b. Rock Quality Designation, RQD This value is expressed in percent and is an indirect measure of rock soundness. It is obtained by summing the total length of all core pieces which are at least four inches long, and then dividing this sum by the total length of the core run.
- 11. Gradation when tests are performed, the percentage of each particle size is listed in the appropriate column (defined in Item 9c).
- 12. When a test is performed to determine the natural moisture content, liquid limit moisture content, or plastic limit moisture content, the moisture content is indicated graphically.
- 13. The corrected standard penetration (N_{60}) value in blows per foot is indicated graphically.

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	BOBING: DI AN	DRAWN	09 00	
FKA-BIXBY KUAU		BEM	30 120	
PID N0.82404	BIXBY ROAD	TAH	HORIZONTAL SCALE IN FEET	

Client: Franklin County Engineer						er		Project: Winchester Pike at Bixby-Brice					Job No. 1121-1010.00								
LOG OF: Boring B-1 Location						Loc	cation	n: As per plan Date Drilled: 1					0/31/2011 to 10/31/2011								
Depth (ft)	Elev. (ft)	Blows per 6"	Recovery (in)	Sam No	Press / Core d	Hand Penetro- meter (tsf)	WATER OBSERVATIONS: G and Water seepage at: 8.5-10.0' water level at completion: None observed eter FIELD NOTES:							% Sit 01	% Clay	STAN Natu Blows ₁ 1	IDARD ral Moi L ⊢— per foot 0	$\frac{PENI}{sture}$	ETRAT Conte / Non- 30	TION ent, % → L Plastic 40	(N60) - ♥ L :- NP
0.2 /	760.3/	3		1		15	Т	opsoil - 2" //	夼	$\overline{1}$	31 1	2	. 12	25	5 21						
<u>1.5</u> -	759.0	6 3 3 4	10 10	2		2.5	FI da St	LL: Stiff brown SANDY SILT (A-4a), some gravel, some clay; amp/ iff to very stiff brown SILT AND CLAY (A-6a), some gravel,			29	7	10	28	3 26	$\begin{array}{c} & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ \end{array}$. + + + + ₽ 		
-		2 3	14	3		1.0	litt @	le fine to coarse sand; damp to moist. 3.0'-4.5', brown and gray mottling.													
-		3 4 5	18	4		2.0											, , ,				
-		5 5	18	5		2.0															
8.5	752.0	9	1	6			M	edium dense brown FINE SAND (A-3), little silt; wet.													
								Bottom of Boring - 10.0'													

Client:	Fran	klin C	Count	y Eng	line	er		Project: Winchester Pike at Bixby-Brice							Job No. 1121-1010.00
LOG	DF: Bo	oring	B-2			Loc	cation	: As per plan		D	ate	Dri	illec	<i>d:</i> 10	0/31/2011 to 10/31/2011
Depth (ft)	Elev. (ft)	Blows per 6"	Recovery (in)	Sam No	Press / Core	Hand Penetro- meter (tsf)	WATI FIELL	ER OBSERVATIONS: Water seepage at: 8.5-10.0' Water level at completion: None observed NOTES: DESCRIPTION	Graphic Loa	% Aggregate	W N. Sand	% F. Sand	% Sit 01	% Clay	STANDARD PENETRATION (N60) Natural Moisture Content, % - ♥ PL → ↓ LL Blows per foot - ○ / Non-Plastic - NP 10 20 30 40
0.3 /	753.4/	1		1		0.75	Т	opsoil - 4"	\rightarrow	0 3	3	. 12	30	9 46	
<u>1.5</u> -	752.2	5 1 4 5	10 18	2		1.0	M sa M	edium stiff dark gray ORGANIC CLAY (A-8b), little coarse ind; moist.		5 2	2	10	36	6 47	
-		3 3 3	18	3		0.75	cc	arse sand, trace fine gravel; moist.							
<u>5</u> 6.0	747.7	4 2 3	6	4		0.25	@	4.5'-6.0', moist to wet.	-						
-		⁴ 8 9	10	5			M fin	edium dense brown COARSE AND FINE SAND (A-3a), little e gravel, little silt; wet.							
8.5 - 10.0 10	745.2	12 5 4	18	6			Lo	oose gray FINE SAND (A-3), little silt, trace fine gravel; wet.							
- - - - - - - - - - - - - - - - - - -								Bottom of Boring - 10.0'							

DLZ Ohio, Inc. * 6121	1 Huntley Road, Columbus	, Ohio 43229 *	(614) 888-0040
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Client:	Fran	klin C	Count	y Eng	inee	ər	Project: Winchester Pike at Bixby-Brice								Job N	<i>lo.</i> 112	1-101	0.00	
LOG	DF: Bo	oring	B-3			Loc	cation: As per plan			Da	ite	Drill	led	: 1/	5/2012	to 1/5/	2012		
Depth (ft)	Elev. (ft)	Blows per 6"	Recovery (in)	Sam No	Press / Core	Hand Penetro- meter (tsf)	WATER OBSERVATIONS: Water seepage at: 7.9-10.5' Water level at completion: None observed FIELD NOTES: DESCRIPTION	Graphic Log	% Aggregate	GR C. Sand B	% M. Sand D	% F. Sand	% Siit 0	% Clay	STAN Natur PL Blows p 1(DARD F al Mois er foot -) 20	$\frac{PENET}{ture Co}$	RATION ontent, % on-Plasti 80 4	(N60) 6 - ♥ LL c - NP 0
-		4 7 11 4 4	7	1 2		1.25 2.0	Stiff to very stiff gray SILT AND CLAY (A-6a), some fine to coarse sand, some fine gravel; moist.		34 21	15 8		14 14	20 32	18 25					
<u>3.0</u> - <u>5</u>	749.4	5 7 17 40 6 7	12	3		2.75	Stiff to very stiff gray SILTY CLAY (A-6b), little fine to coarse sand, trace fine gravel; moist.									+++++ 	++++ 		
- - 7.9	744.5	7 4 5 6 3	16 18	5		2.25													
9.0 10.5	743.4	6 12 11 15	12 7	6A/B 7		1.0/NA	Medium dense brown COARSE AND FINE SAND (A-3a), little silt, little fine gravel; wet. Medium dense brown GRAVEL (A-1-a), little fine to coarse sand, trace silt; wet.												
10.5 - - - - - - - - - - - - - - - - - - -	741.9	15	7				sand, trace silt; wet. Bottom of Boring - 10.5'	0 /									$\begin{array}{c} \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\$		

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Client	: Fran	klin C	count	y Eng	line	er		Project: Winchester Pike at Bixby-Brice								Job	No.	1121	-101	10.00)	
LOG	OF: Bo	oring	B-4			Loc	catior	<i>:</i> As per plan			Da	ate	Dril	llea	1: 1/	5/201	2 to	1/5/2	2012			
Depth (ft)	Elev. (ft)	Blows per 6"	Recovery (in)	Sam No	Press / Core	Hand Penetro- meter (tsf)	FIEL	ER OBSERVATIONS: Water seepage at: 6.3-9.0' Water level at completion: 13.8' D NOTES: DESCRIPTION	Graphic Log	% Annrenate	% C. Sand	% M. Sand D	% F. Sand	% Sitt 0	% Clay	STA Nat Blows	NDA ural PL s per 10	RD P Moisti foot -	ENET Jre C	RAT onter Non-P	ION (nt, % ⊣ Li lastic 40	<i>'N60)</i> - ♥ L
	-	1 2 WOH 2 3 1 3	13 7	1 2 3		1.25 1.25 1.0	Si tra	iff to very stiff dark gray CLAY (A-7-6), little coarse sand, ace gravel; organic; damp to moist.		3	i 1 i 1		7 6	41 43	42 46							
<u>4.8</u>	747.0	WOH WOH WOH 2 3	16	4 5				ery soft gray SILT (A-4b), trace fine to coarse sand; wet.	+ + + + + + + + + + + + + + + + + + + +	- 0	1		6	63	29					-1: -1: -1: -1:		
7.5	744.3	2 WOH 2 3	9 10	6		1.25	fir M cc	edium stiff brown SILT AND CLAY (A-6a), some fine to barse sand, trace to little fine gravel; moist; contains wet sand	· <u>O</u> .								 					
<u>10</u>)	5 7 2	18	7		1.5		20113.														
		4 4 2	16	8		1.25																
15.5 15	736.3	47	18	9		2.5											þ					
2 <u>(</u>								Bottom of Boring - 15.5'														

Client:	Fran	klin C	Count	y Eng	inee	er		Project: Winchester Pike at Bixby-Brice							Job N	o. 112	1-1010	0.00	
LOG	DF: Bo	oring	B-5			Loc	ation	: As per plan		D	ate	Dri	illea	1: 1/	5/2012	to 1/5/	2012		
Depth (ft)	Elev. (ft)	Blows per 6"	Recovery (in)	Sam No	Press / Core	Hand Penetro- meter (tsf)	WATI FIELL	ER OBSERVATIONS: Water seepage at: 4.8-10.5' Water level at completion: 6.7' D NOTES: DESCRIPTION	Graphic Log	% Aggregate	W W. Sand Band	% F. Sand	% Siit 01	% Clay	STANI Natur Blows pu	DARD P al Moist i	$ent{ENETF}$	RATIOI ntent, on-Plas	N (N60) % - • LL tic - NP 40
1.5	755.9	3 4 4	12	1		1.25	M cc	edium stiff brown SILT AND CLAY (A-6a), some fine to arrse sand, trace fine gravel; moist.		1 9	9	14	40	36		N	<u>, , , , , , , , , , , , , , , , , , , </u>		
		4 4 5	16	2		2.75	St tra	iff brown SILTY CLAY (A-6b), some fine to coarse sand, ace fine gravel; moist.		2 9	9	15	33	3 41		 	 ♥ 		
- 4.8 _ 5	752.6	3 4 4 1	15	3		2.0													
<u>6.1 _</u>	751.3	2 2 2	16	4			M sa	edium stiff brown SILTY CLAY (A-6b), "and" fine to coarse nd, trace fine gravel; wet.	• •	4 2	3	23	22	2 28		 - 		+ @ + 	
-		4 4 3	10	5			Lo S/	AND (A-3a), little fine gravel, trace silty clay; wet.											
-		8 10 5	18	6				•	\vdots										
10.5 ¹⁰	746.9	8 12	16	7				Bottom of Boring - 10.5'	<u>···</u>								DI I I DI I I I I I I		
- - - - - - - - - - - - - - - - - - -								Bolion of Bonng - 10.3											

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Client:	Fran	klin C	Count	y Eng	line	er		Project: Winchester Pike at Bixby-Brice		-					Job	No. 1	121-	101(00.0		
LOG	DF: Bo	oring	B-6			Loc	cation	: As per plan			Dat	e D	rille	<i>d:</i> 10	0/31/2	011 t	o 10	/31/2	2011		
Depth (ft)	Elev. (ft)	Blows per 6"	Recovery (in)	Sam No enuc	Press / Core	Hand Penetro- meter (tsf)	FIELD	ER OBSERVATIONS: Water seepage at: 8.5-10.0' Water level at completion: None observed D NOTES: DESCRIPTION	Graphic Log	% Aggregate	RA C. Sand	% M. Sand VO	% F. Sand % cit	% Clay ≥	STA Nat Blows	NDAR ural M PL ⊢ per fo 10	PD PE loistui ot - (20	NETF re Co 	RATIC Intent, On-Pla	0N (N6 % - LL stic - N 40	; 0) ♥
0.5	760.2	2 3		1		2.5	Тс	ppsoil - 6"		7	7.	1	3 3	7 36							
<u>1.5</u> -	759.2	4 1 2	13	2		1.0	FI sa	LL: Very stiff brown SILTY CLAY (A-6b), some fine to coarse ind, trace fine gravel; moist.		12	9.	1	4 3	6 29		 					
- 4.5	756.2	3 41 43	15 2	3			FI litt @	LL: Stiff brown SILT AND CLAY (A-6a), some fine gravel, le gravel; moist. 3.0'-4.5', concrete fragments encountered.												 	 ++- 1 10
<u>5</u> 6.0	754.7	12 8 6	18	4		3.0	Ve litt	ery stiff brown SILTY CLAY (A-6b), some fine to coarse sand, le fine gravel; damp.									 	 			 ++-
-		1 3 4	10	5			Lc (A	pose brown GRAVEL WITH SAND, SILT, AND CLAY -2-6), little silty clay, little fine gravel; moist to wet.	0.												
8.5	752.2	10																			
- 10.0 10	750.7	9 9	18	6			fin	e gravel, trace silty clay; moist.										 D			
- - <u>15</u> - - <u>20</u> - - - - - - - -								Bottom of Boring - 10.0'													

Client:	Fran	klin C	count	y Eng	line	er		Project: Winchester Pike at Bixby-Brice							Job No. 1121-1010.00
LOG	DF: Bo	oring	B-7			Loc	cation	: As per plan		D	ate	Dri	illeo	d: 1/	/5/2012 to 1/5/2012
Depth (ft)	Elev. (ft)	Blows per 6"	Recovery (in)	Sam No Prive	Press / Core	Hand Penetro- meter (tsf)	WATI FIELL	ER OBSERVATIONS: Water seepage at: 9.2-10.5' Water level at completion: 6.5' O NOTES: DESCRIPTION	Graphic Log	% Aggregate	W Sand	% F. Sand	% Silt 01	% Clay	STANDARD PENETRATION (N60) Natural Moisture Content, % - ♥ PL ⊢ LL Blows per foot - ○ / Non-Plastic - NP 10 20 30 40
1.5	758.0	1 3 3	18	1		1.25	St	iff brown SILT AND CLAY (A-6a), little coarse sand; moist.		0 4	۰	- 14	48	3 33	
-		2 3 5	14	2		2.0	Ve tra	ery stiff brown SILTY CLAY (A-6b), little fine to coarse sand, ace to little fine gravel; moist.		1 4	۰	- 16	3	5 43	
4.5	755.0	4 7 6	18	3		2.25									
-		8 11 6	17	4		4.5	sa	nd, trace to little fine gravel; damp.							
-		8 10 4	6	5		2.5		6.0 - 7.5 , single large piece of graver recovered.							
9.2 -	750.3	8 14 4	6	6		2.0			• •						
10.5 10.5 - - - - - - - - - - - - -	749.0	8 10	14	7			M. fin	edium dense gray COARSE AND FINE SAND (A-3a), trace e gravel, trace silt; wet. Bottom of Boring - 10.5'							

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Client: Franklin County Engineer							Project: Winchester Pike at Bixby-Brice									Job No. 1121-1010.00						
LOG	DF: Bo	oring	B-8			Loc	ation	z: As per plan			Da	ate	Dril	llea	1: 10)/31/20	011 to	10/31	/2011			
Depth (ft)	Elev. (ft)	Blows per 6"	Recovery (in)	Sam No	Press / Core	Hand Penetro- meter (tsf)	WAT.	ER OBSERVATIONS: Water seepage at: None observed Water level at completion: None observed D NOTES: DESCRIPTION	Graphic Loa	0, Accession (% Aggregate % C. Sand <u></u>	% M. Sand D	% F. Sand	% Siit 0	% Clay	STAN Natu Blows	IDARD ral Mois L I Hor Der foot	PENE sture C	TRATI Conten Non-Pl 30	ON (I t, % - ⊣ LL astic - 40	160) . () . NP	
0.1	754.9	3		1			\ Τo	opsoil - 1" /	0	5	2 22		12	1	5							
1.5	753.5	4 3 2 3	5 3	2		1.0	FI sa M	LL: Loose brown GRAVEL (A-1-a), some fine to coarse and, little silty clay; damp. edium stiff dark gray to gray CLAY (A-7-6), little fine to coarse			0 8		11	39	32			 ⊕ 				
- <u>5</u>		3 2 3 2	15	3		1.0	Sa	and, trace gravel; organic; moist.														
6.0	749.0	23	10	4		0.75																
-		1 2 3	15	5		0.75	M fir	edium stiff to stiff brownish gray SILTY CLAY (A-6b), some ne to coarse sand, trace fine gravel; moist.														
- 10.0 10	745.0	3 4 5	10	6		1.5																
- - - - - - - - - - - - - - - - - - -								Bottom of Boring - 10.0'														

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Client:	Fran	klin C	count	/ Eng	inee	er		Project: Winchester Pike at Bixby-Brice								Job No. 1121-1010.00
LOG	DF: Bo	oring	B-9			Loc	catior	z: As per plan			D	ate	Dri	llec	<i>d:</i> 10	0/31/2012 to 10/31/2012
Depth (ft)	Elev. (ft) 761.8	Blows per 6"	Recovery (in)	Sam, No	Press / Core	Hand Penetro- meter (tsf)	WAT FIEL	ER OBSERVATIONS: Water seepage at: None observed Water level at completion: None observed D NOTES: DESCRIPTION	Crashio Loc	diapilic rog	% Aggregate	% M. Sand	% F. Sand	% Silt 01	% Clay	STANDARD PENETRATION (N60) Natural Moisture Content, % - ♥ PL → ↓ LL Blows per foot - ○ / Non-Plastic - NP 10 20 30 40
0.3 /	761.6/	2 3		1		3.0	G	ravel - 3" //	亻		8 1	0	13	38	3 30	
<u>1.5</u> -	760.3	3 3 6 3	10 10	2		1.0	P cl S	OSSIBLE FILL: Very stiff brown SANDY SILT (A-4a), some ay, trace gravel; damp/ tiff brown SANDY SILT (A-4a), some clay, trace gravel; damp.			8 1	4	15	36	6 27	
-	-	4 2 3	18	3		1.0										
		4 7	18	4		1.75										
7.0	754.8	6 7 9	18	5		4.5	a) 6.0', hard.								
-	-	Q					v sa	ery stiff to hard brown SILTY CLAY (A-6b), little fine to coarse and, trace fine gravel; damp to moist.								$\left \begin{array}{cccccccccccccccccccccccccccccccccccc$
- 10.0 10	751.8	8 10	18	6		3.0										
- - - - - - - - - - - - - - - - - - -								Bottom of Boring - 10.0'								

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Client: Franklin County Engineer								Project: Winchester Pike at Bixby-Brice								Job No. 1121-1010.	00
LOG	DF: Bo	oring	B-1(0		Loc	catior	n: As per plan			Da	te I	Dril	llea	1: 10	/31/2011 to 10/31/20)11
Depth (ft)	Elev. (ft)	Blows per 6"	Recovery (in)	Sam No Puive	Press / Core	Hand Penetro- meter (tsf)	WAT FIELI	ER OBSERVATIONS: Water seepage at: None observed Water level at completion: None observed D NOTES: DESCRIPTION	Graphic Log	% Aggregate	GR C. Sand	% M. Sand D	% F. Sand TA	<u>% Silt</u>	% Clay	STANDARD PENETRA Natural Moisture Con PL H Blows per foot - O / Nor 10 20 30	ATION (N60) tent, % - ● → LL 1-Plastic - NP 40
0.2 /	763.9/	2 4		1		1.0	Т	opsoil - 2"		22	7		11	30	30		
-		3 2 4 3	12 14	2		2.0	S	tiff to very stiff brown SILTY CLAY (A-6b), trace to little fine to barse sand, trace fine gravel; moist.		7	5		12	41	35		● ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓
-		5 5	18	3		2.0											
_5		6 7	18	4		2.0				-							
-		6 7 7	18	5		3.75											
8.5 -	755.6																
-	754 1	11 8 6	15	6			M fir	ledium dense brown GRAVEL WITH SAND (A-1-b), some ne to coarse sand, trace to little silty clay; moist.	0.								
								Bottom of Boring - 10.0'									

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Client:	Client: Franklin County Engineer							Project: Winchester Pike at Bixby-Brice								Job No. 1121-1010.00						
LOG	DF: Bo	oring	B-11	1		Loc	cation	: As per plan			Ľ	ate	Dri	llec	<i>d:</i> 1()/31/20	011 to	10/31	1/201	1		
Depth (ft)	Elev. (ft)	Blows per 6"	Recovery (in)	Sam No	Press / Core	Hand Penetro- meter (tsf)	WATI FIELL	ER OBSERVATIONS: Water seepage at: 8.5-10.0' Water level at completion: None observed D NOTES: DESCRIPTION		ы старпіс Log	% Aggregate	% M. Sand 8	% F. Sand	% Silt 01	% Clay	STAN Natu Blows	IDARD ral Mois L I I I I I I I I I I I I I I I I I I I	PENE sture ($- \bigcirc /$	TRAT Conte	TION ent, % ⊣ L Plastic 40	(N60) - ♥ L - NP	
0.2 /	765.4/	2		1		1.0	Т	opsoi - 2"	$\overline{\mathcal{V}}$	\geq	10	6	- 13	45	27							
-	-	4 1 2 4	18 18	2		1.5	St fir	iff to very stiff brown SILT AND CLAY (A-6a), little to some e to coarse sand, trace fine gravel; moist.			3	6	- 14	42	2 35				 			
-		2 3 4	15	3		2.0																
		5 6	18	4		1.0																
-		6 5	18	5		3.0	a a	6.0'-7.5', little fine gravel.														
8.5	757.1	5								<u> </u>												
- 10.0 10	755 6	6 5	18	6			IVI fir	edium dense brown GRAVEL WITH SAND (A-1-b), some e to coarse sand, trace to little silty clay; moist.	· 2	2.5												
- - - - - - - - - - - - - - - - - - -								Bottom of Boring - 10.0'														

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Client: Franklin County Engineer								Project: Winchester Pike at Bixby-Brice								Job No. 1	121-1	1010.0	00	
LOG	OF: Bo	oring	C-1			Lo	catior	n: As per plan	Date Dril)/31/2011 t	o 10/3	31/20 ⁻	11	
Depth (ft)	Elev. (ft)	Blows per 6"	Recovery (in)	Sam Nc enive	Press / Core	Hand Penetro- meter (tsf)	FIEL	ER OBSERVATIONS: Water seepage at: None observed Water level at completion: None observed D NOTES: DESCRIPTION	Graphic Log	% Aggregate	% C. Sand	% M. Sand	% F. Sand X	% Siit	% Clay	STANDAR Natural M PL ⊢ Blows per for 10	TION (N60) ent, % - ♥ → LL -Plastic - ℕP 40			
		E					A	sphalt=16" Bottom of Boring - 1.3'			0	δ ΄	<u><u><u></u></u></u>	8	0					

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Client:	Fran	klin C	count	y Eng	inee	er		Project: Winchester Pike at Bixby-Brice				Job No. 1121-1010.00								
LOG	DF: Bo	oring	C-2			Loc	catior	n: As per plan			Da	te	Dril	llea	1: 10	0/31/2	011 to	10/31/	2011	
Depth (ft)	Elev. (ft)	Blows per 6"	Recovery (in)	Sam No	Press / Core	Hand Penetro- meter (tsf)	FIEL	ER OBSERVATIONS: Water seepage at: None observed Water level at completion: None observed D NOTES: DESCRIPTION	Graphic Log	% Aggregate	C. Sand B	% M. Sand D	% F. Sand	% Siit 0	% Clay	STAI Natu F Blows	VDARD ıral Moi ⊵L ⊢— per foot 10	PENET sture Co	RATIOI ontent, lon-Plas	N (N60) % - ● LL ttic - NP 40
	100.1		_				A	sphalt=9.5"/Brick=3.5"/Concrete=6"												
								Bottom of Boring - 1.6'												

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Client	Fran	klin C	count	y Eng	line	er		Project: Winchester Pike at Bixby-Brice								Job No. 1121-1010.00		
LOG	OF: Bo	oring	C-3			Loc	cation	z: As per plan			Dat	te D	Drille	rilled: 10/31/2011 to 10/31/2011				
Depth (ft)	Elev. (ft)	Blows per 6"	Recovery (in)	Sam No Duive	Press / Core	Hand Penetro- meter (tsf)	WATI FIELL	ER OBSERVATIONS: Water seepage at: None observed Water level at completion: None observed D NOTES: DESCRIPTION	Graphic Log	% Aggregate	% C. Sand	% M. Sand	% F. Sand		% Clay	STANDARD PENETRATION (N60) Natural Moisture Content, % - ♥ PL → LL Blows per foot - ○ / Non-Plastic - NP 10 20 30 40		
0.5							As	sphalt= 5.5"/Aggregate base Bottom of Boring - 0.5'										

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Client.	Fran	klin C	count	y Eng	inee	er		Project: Winchester Pike at Bixby-Brice								Job	No. 11	21-10	10.00	
LOG	DF: Bo	oring	C-4			Loc	cation	z: As per plan			Da	te	Dri	llec	ed: 10/31/2011 to 10/31/2011					
Depth (ft)	Elev. (ft)	Blows per 6"	Recovery (in)	Sam No	Press / Core	Hand Penetro- meter (tsf)	FIELL	ER OBSERVATIONS: Water seepage at: None observed Water level at completion: None observed D NOTES: DESCRIPTION	Graphic Log	% Aggregate	% C. Sand	% M. Sand D	% F. Sand	% Sit 0	% Clay	STA Nai Blows	NDARD Tural Moi PL I s per foot 10	PENE	TRATI Conten Non-Pl 30	ON (N60) t, % - ● + LL astic - NP 40
1.0	760.7	-					A	sphalt=6"/Aggregate=6"			-	-		_	-					
								Bottom of Boring - 1.0'												

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Client:	Franl	klin C	ount	y Eng	ine	ər		Project: Winchester Pike at Bixby-Brice								Job No	. 112	1-10	10.00	
LOG	DF: Bo	oring	C-5			Lo	catior	n: As per plan		l	Dat	te I	Drille	Job No. 1121-1010.00 Drilled: 10/31/2011 to 10/31/2011						
Depth (ft)	Elev. (ft)	Blows per 6"	Recovery (in)	Sam Nc	Press / Core	Hand Penetro- meter (tsf)	FIEL	ER OBSERVATIONS: Water seepage at: None observed Water level at completion: None observed D NOTES: DESCRIPTION	Graphic Log	% Aggregate	% C. Sand	% M. Sand D	% F. Sand A	% Siit 0	% Clay	STAND, Naturai PL Blows per 10	ARD F Mois foot - 20	$\frac{PENE}{ture}$	TRATIC Content Non-Pla 30	DN (N60) , % - ♥ LL stic - NP 40
		-					A	sphalt=9"/Concrete=10"												
	757.8							Bottom of Boring - 1.6'												

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Client:	Fran	klin C	count	y Eng	inee	er		Project: Winchester Pike at Bixby-Brice								Job I	Vo. 112	21-101	0.00	
LOG	DF: Bo	oring	C-6			Loc	catior	n: As per plan			Dat	te L	Drille	ed.	: 10)/31/20	11 to	10/31/2	2011	
Depth (ft)	Elev. (ft)	Blows per 6"	Recovery (in)	Sam No	Press / Core	Hand Penetro- meter (tsf)	FIEL	ER OBSERVATIONS: Water seepage at: None observed Water level at completion: None observed D NOTES: DESCRIPTION	Graphic Log	% Aggregate	% C. Sand	% M. Sand	% F. Sand	% Sit 0	% Clay	STAN Natu Blows p 1	DARD ral Mois ber foot - 0 2	PENET sture Co 0 / N	RATIOI ontent, on-Plas	N (N60) % - ● LL tic - NP 40
	100.1						A	sphalt=9"/Brick=3.5"/Concrete=6.5"												
								Bottom of Boring - 1.6'												

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Client:	Franl	klin C	ount	y Eng	inee	er		Project: Winchester Pike at Bixby-Brice								Job No	. 112	1-10	10.00	
LOG	DF: Bo	oring	C-7			Lo	catior	n: As per plan			Da	te	Dril	llea	1: 10	0/31/201	1 to 1	0/31	2011	
Depth (ft)	Elev. (ft)	Blows per 6"	Recovery (in)	Sam _i No	Press / Core	Hand Penetro- meter (tsf)	FIEL	ER OBSERVATIONS: Water seepage at: None observed Water level at completion: None observed D NOTES: DESCRIPTION	Graphic Log	% Aggregate	GR C. Sand	% M. Sand D	% F. Sand	% Silt 0	% Clay	STAND, Natural PL Blows per 10	ARD F Mois I foot - 20	$\frac{PENE}{ture C}$	「RATIC content, ────↓ Non-Pla 30	0N (N60) % - ● LL stic - NP 40
0.9	763.9	_	_				A	sphalt=2"/Concrete=8.5"												
0.0 - - - - - - - - - - - - -								Bottom of Boring - 0.9'												

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Client	: Fran	klin C	Count	y Eng	ine	er		Project: Winchester Pike at Bixby-Brice								Job	Vo. 11	21-1	010.0	0	
LOG	OF: Bo	oring	C-8			Lo	catior	n: As per plan			Da	te	Dril	lled	1: 10)/31/20	011 to	10/3	1/201	1	
Depth (ft)	Elev. (ft) 763.6	Blows per 6"	Recovery (in)	Sam No	Press / Core	Hand Penetro- meter (tsf)	FIEL	ER OBSERVATIONS: Water seepage at: None observed Water level at completion: None observed D NOTES: DESCRIPTION	Graphic Log	% Aggregate	R C. Sand	% M. Sand D	% F. Sand	% Silt 0	% Clay	STAI Natu F Blows	IDARD Iral Mol IL I per foot	PENI isture	ETRA Conte / Non-1 30	TION (ent, % → Li Plastic 40	(N60) - ♥ L 2- NP
<u>1.4</u>	763.6 762.2 762.2 762.2 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7							sphalt=9"/Aggregate=8" Bottom of Boring - 1.4'			<u> </u>				<u>6</u>						

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Client: Franklin County Engineer Project: Winchester Pike at Bixby-Brice														Job No. 1121-1010.00						
LOG	DF: Bo	oring	C-9			Loc	cation	z As per plan		Da	te l	Drill	led	: 10	0/31/2011 to 10/31/2011					
Depth (ft)	Elev. (ft)	ows per 6"	ecovery (in)	Sam, No	ess / Core	Hand Penetro- meter (tsf)	FIELL	ER OBSERVATIONS: Water seepage at: None observed Water level at completion: None observed D NOTES:	aphic Log	Aggregate	C. Sand	M. Sand D	E. Sand	Silt	Clay	STANE Natura PL Blows pe	DARD I al Mois i	PENET	RATIO ontent, Non-Pla	N (N60) % - ♥ LL stic - NP
	763.4	B	Ř	à	à	()		DESCRIPTION	Ğ	%	%	%	%	%	%	10	2	0	30	40
	762.2							Bottom of Boring - 1.3'												



Project: Winchester Pike at Bixby-Brice Project No: 1121-1010.00



3RAIN SIZE II - DLZ MOD - GINT STD US LAB. GDT - 2/9/12 14:22 - S: DEPTI/GEOTECHNICAL/GINT/PROJECTS/1121-1010.00 WINCHESTER PIKE AT BIXBY-BRICE.GPJ



1

Client: Franklin County Engineer Project: Winchester Pike at Bixby-Brice Project No: 1121-1010.00



3RAIN SIZE II - DLZ MOD - GINT STD US LAB.GDT - 2/9/12 14:23 - S: DEPTIGEOTECHNICAL/GINT/PROJECTS/1121-1010.00 WINCHESTER PIKE AT BIXBY-BRICE.GPJ



3RAIN SIZE II - DLZ MOD - GINT STD US LAB.GDT - 2/9/12 14:23 - S: DEPTIGEOTECHNICAL/GINT/PROJECTS/1121-1010.00 WINCHESTER PIKE AT BIXBY-BRICE.GPJ



3RAIN SIZE II - DLZ MOD - GINT STD US LAB.GDT - 2/9/12 14:23 - S: DEPTIGEOTECHNICAL/GINT/PROJECTS/1121-1010.00 WINCHESTER PIKE AT BIXBY-BRICE.GPJ



EXAMPLE

Client: Franklin County Engineer Project: Winchester Pike at Bixby-Brice Project No: 1121-1010.00





1

Client: Franklin County Engineer Project: Winchester Pike at Bixby-Brice Project No: 1121-1010.00



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Client: Franklin County Engineer **Project:** Winchester Pike at Bixby-Brice

Project No: 1121-1010.00



Project: Winchester Pike at Bixby-Brice

Project No: 1121-1010.00



3RAIN SIZE II - DLZ MOD - GINT STD US LAB. GDT - 2/9/12 14:25 - S: DEPTIGEOTECHNICAL/GINT/PROJECTS/1121-1010.00 WINCHESTER PIKE AT BIXBY-BRICE.GPJ





3RAIN SIZE II - DLZ MOD - GINT STD US LAB. GDT - 2/9/12 14:25 - S: DEPTIGEOTECHNICAL/GINT/PROJECTS/1121-1010.00 WINCHESTER PIKE AT BIXBY-BRICE.GPJ



DLZ MOD - GINT STD US LAB. GDT - 2/9/12 14:25 - S: DEPTIGEOTECHNICAL/GINT/PROJECTS/1121-1010.00 WINCHESTER PIKE AT BIXBY-BRICE.GPJ **GRAIN SIZE II -**



Project: Winchester Pike at Bixby-Brice

Figure

Project No: 1121-1010.00

3RAIN SIZE II - DLZ MOD - GINT STD US LAB. GDT - 2/9/12 14:25 - S: DEPTIGEOTECHNICAL/GINT/PROJECTS/1121-1010.00 WINCHESTER PIKE AT BIXBY-BRICE.GPJ



Project: Winchester Pike at Bixby-Brice Project No: 1121-1010.00

Figure

3RAIN SIZE II - DLZ MOD - GINT STD US LAB. GDT - 2/9/12 14:25 - S: DEPTIGEOTECHNICAL/GINT/PROJECTS/1121-1010.00 WINCHESTER PIKE AT BIXBY-BRICE.GPJ



Project: Winchester Pike at Bixby-Brice

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ODLZ

Project: Winchester Pike at Bixby-Brice Project No: 1121-1010.00



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Client: Franklin County Engineer Project: Winchester Pike at Bixby-Brice





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DLZ Client Proje Proje

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Subgrade Analysis			G	lobal Op		Classification Counts by Sample												Surface Class	% Bor	rings	% Surface		Rig	ER					
			320 R&R		N	0	R	1a	1b	3	3a	2-4	2-5 2-6	5 2-7	4a	4b	5 6a	6b	7-5	7-6	8a	8b	2-5 0	N _{60L} <= 5	18%	82	%	А	79
V. 12.00 12/30/11			206	CS		2	0	0	1	0	0	0	0 1	0	0	1	0 1	37	0	0	0	3	4b 1 9%	<=10	100%	18%	82%	в	66
Destau			LS			00/		2%		EQ	/	2%			2%	2%	84%	0/			7%	5 0	>=20	0%			C		
CBP 6		206	LKU (0%				57	0			-			957	/o				7-5 0	IVI+	0%			F		
CDN -		200	Deptil	•							N ₆₀ N ₆₀			ΡI	Clay	,	М Морт			GI	7-0 0 8a 0		0 /8			F			
Total Borings 11									Avera	qe		ſ	13.4 6.	8	1		i 🗂	٦		15.4		9.66	8b 1 9%			21.4		G	
PID 82404								Maxim	num		Ē	111 10							16		10	R 0			36		н		
Location FRA-		-Bixby "E	ast Alt. /	-			Minim	um			0 0							6		0		·		16					
		Borin	g				Sub	grade		Stan	dard P	enetra	ation		Physic	cal Ch	aracteristic	s	Mois	sture	Cl	ass	Comments	Probl	lem	Unde	rcuts	Ar	nalysis
						Cut											% %	Р			Ohio			w/	w/	UC	UC		
#	B #	Boring Loca	tion	Depth	То	Fill	Depth	n To	n ₂	n ₃	Ν	Rig	N ₆₀ N ₆₀	LL	PL	PI	Silt Clay	200	М	M _{OPT}	DOT	GI		Class	MN	Class	MN		
																		_		1									
1	B-1	As per plan		0.0	1.5	0.5	0.5	2.0	2	4	6	A	8							10	4b	10		4b	N	36	18		
				1.5	3.0		2.0	3.5 5.0	2	4	6 7		8							16	6D 6b	10			IN N		18		
				4.5	6.0		5.0	6.5	5	6	11		14	8						16	6b	10			MN		10		
2	B-2	As per plan		0.0	1.5	0.0	0.0	1.5	2	5	7	А	9	-						16	6b	10			N		16		
				1.5	3.0		1.5	3.0	4	5	9		12							16	6b	10			MN				
1				3.0	4.5		3.0	4.5	3	3	6		8							16	6b	10			N		18		
<u> </u>	5.0			4.5	6.0	0.5	4.5	6.0	2	3	5	-	7	7						16	6b	10		<u> </u>	N		21		
3	B-3	As per plan		0.0	1.5	2.5	2.5	4.0		11	18	В	20							16	6b 6b	10			N		15		
				1.5	3.0 4.5		4.0	5.5 7.0	4	5 40	9 57		10							16	6b	10			IN		15		
				4.5	6.0		7.0	8.5	7	7	14		15 1	0						16	6b		Diove graver						
4	B-4	As per plan		0.0	1.5	3.5	3.5	5.0	2	3	5	В	6	-							8b			Un	Ν	36/All	24		
				1.5	3.0		5.0	6.5	2	3	5		6								8b			Un	N	36/All	24		
				3.0	4.5		6.5	8.0	3	3	6		7								8b			Un	N	36/All	21		
	5.5			4.5	6.0		8.0	9.5	0	0	0	-	0	0						16	6b				N		48		
5	B-5	As per plan		0.0	1.5	2.0	2.0	3.5	4	4	8	В	9							16	6b 6b	10			N		16		
				1.5	3.0 4.5		5.0	5.0 6.5	4	5 4	9		10 Q							16	6b	10			N		15		
				4.5	6.0		6.5	8.0	2	2	4		4	4						10	2-6	10			N		30		
6	B-6	As per plan		0.0	1.5	1.0	1.0	2.5	3	4	7	А	9							16	6b	10			Ν		16		
				1.5	3.0		2.5	4.0	2	3	5		7							16	6b	10			N		21		
				3.0	4.5		4.0	5.5	41	43	84		111	_						16	6b	10	Drove gravel						
-	B 7	As per plan		4.5	6.0	0.0	5.5	1.0	8	6	14	P	18	/						16	6b	10			N		21		
'	B-7	As per plan		1.5	3.0	0.0	1.5	3.0	3	5	0 R	D	9							16	6b	10			N		21 16		
1				3.0	4.5		3.0	4.5	4	7	11		12							16	6b	10			MN		.5		
1				4.5	6.0		4.5	6.0	8	11	19		21	7						16	6b	10							
8	B-8	As per plan		0.0	1.5	0.5	0.5	2.0	4	4	8	А	11							6	1b	0			Ν				
				1.5	3.0		2.0	3.5	2	3	5		7							16	6b	10			N		21		
				3.0	4.5		3.5	5.0	2	3	5		7	-						16	6b	10			N		21		
0	B-9	As per plan		4.5	0.0	0.0	0.0	0.5	2	3	5	Δ	/ 8	/						16	60	10			N N		<u>∠</u> 1 19		
9	D-9	As per pian		1.5	3.0	0.0	1.5	3.0	6	3	9	A	12							16	6b	0 10			MN		10		
1				3.0	4.5		3.0	4.5	4	2	6		8							16	6b	10			N		18		
				4.5	6.0		4.5	6.0	4	7	11		14	8						16	6b	10			MN				
10	B-10	As per plan		0.0	1.5	0.0	0.0	1.5	4	3	7	А	9							16	6b	10			N		16		
1				1.5	3.0		1.5	3.0	4	3	7		9							16	6b	10			N		16		
1				3.0	4.5		3.0	4.5	5	5	10		13							16	6b	10			MN				
11	B-11	As per plan		4.5	0.0	0.0	4.5	0.0	0	1	13	Δ	8	9				-		16	6b	10		+	N		18		
	5.11	no per pian		1.5	3.0	0.0	1.5	3.0	2	4	6	A	8							16	6b	10			N		18		
1				3.0	4.5		3.0	4.5	3	4	7		9							16	6b	10			Ν		16		
1				4.5	6.0		4.5	6.0	5	6	11		14	8						16	6b	10			MN				