

June 8, 2017

Columbus Engineering Consultants, Inc.
870 Michigan Avenue
Columbus, Ohio 43215

Attention: Mr. Tom Hedrick, P.E.

Reference: Structure Foundation Exploration – Draft
Borrow Road (T-266) Bridge over Patzer Ditch
Jackson Township, Franklin County, Ohio
CTL Project No. 16050169COL

Dear Mr. Hedrick:

CTL Engineering, Inc. has completed the Structure Foundation Exploration report for the above referenced structure. A pdf copy of the draft report is being submitted.

Thank you for the opportunity to work with you on this project. If you have any questions or need further information, please feel free to contact our office.

Respectfully Submitted

CTL ENGINEERING, INC.

A handwritten signature in black ink, appearing to read "Joe Grani".

Joe Grani, P.E.
Project Engineer

STRUCTURE FOUNDATION EXPLORATION-DRAFT

**BORROR ROAD (T-266) BRIDGE OVER PATZER DITCH
JACKSON TOWNSHIP, FRANKLIN COUNTY, OHIO
CTL PROJECT NO. 16050169COL**

PREPARED FOR:

**COLUMBUS ENGINEERING CONSULTANTS
870 MICHIGAN AVE.
COLUMBUS, OHIO 43215**

PREPARED BY:

**CTL ENGINEERING, INC.
2860 FISHER ROAD
COLUMBUS, OHIO 43204
Phone 614-276-8123
Fax 614-276-6377**

June 8, 2017



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I. EXECUTIVE SUMMARY AND INTRODUCTION

The project involves the replacement of an existing bridge that carries Borrer Road (T266) over Patzer Ditch in Jackson Township, Franklin County, Ohio. It is understood that the replacement structure will be a 36 feet (clear span) by 9 feet (rise) conduit type A, precast reinforced concrete arch sections, supported on spread footings.

Two test borings, identified as B-001-0-16 and B-002-0-16, were drilled for this Structure Foundation Exploration. The borings generally exhibited gravel and/or stone fragments with sand (A-1-b), gravel and/or stone fragments with sand and silt (A-2-4), coarse and fine sand (A-3a), sandy silt (A-4a) or silt and clay (A-6a) soils to the drilled depths. No bedrock was encountered within the drill depths.

It is understood that the foundations for the proposed arch bridge will be constructed about 12.9 to 14.4 feet below the existing roadway grade (Foundation Elevation = 702.42 feet). Medium dense granular deposits or hard cohesive soils were encountered in the test borings at the anticipated foundation level. These soils are considered suitable to support foundations for the proposed structure.

II. GEOLOGY AND OBSERVATIONS OF THE PROJECT

According to the Ohio Department of Natural Resources, *Physiographic Regions of Ohio*, the site lies on the Columbus Lowland region of Southern Ohio Loamy Till Plain.

According to Bedrock Geology Map of Ohio (2006), bedrock below the site consists of Devonian age shale. No bedrock was encountered in the drilled borings.

According to web based mapping from *United States Department of Agriculture, Natural Resources Conservation Service*, the project area contains soils primarily described as Miamian Silty Clay Loam, 12 to 18 percent slopes, eroded (MID2), Sloan Silt Loam, frequently flooded (So), and Kendallville Silt Loam, 2 to 6 percent slopes (KeB) soils. According to the *Soil Survey of Franklin County, Ohio*, these soils exhibit moderately high to high permeability.

According to the ODNR Website, no underground mines have been mapped below the structure. However, active sand, gravel and limestone surface mine operations are performed about 1 mile east of the structure.

According to the Ohio Karst Areas map prepared by the Ohio Department of Natural Resources (ODNR), the project site does not lie in a Probable Karst Area.

Historic geotechnical records were searched for on the ODOT GeoMS website. No historic geotechnical records were found for this site.

III. EXPLORATION

Two (2) structure test borings, designated as B-001-0-16 and B-002-0-16, were drilled to depths ranging from 60.0 to 65.0 feet below grade.

The borings were performed with a track mounted drill rig utilizing hollow stem augers (HSA) on December 19 and 20, 2016. Standard penetration tests were conducted using a 140-pound hammer falling 30 inches to drive a 2-inch O.D. split barrel sampler. The energy transfer ratio associated with the automatic SPT hammer was 81.9 percent. The hammer was calibrated in July 2015.

Soil samples obtained from the drilling operation were preserved in glass jars, visually classified in the field and laboratory, and tested for natural moisture content. Representative soil samples were subjected to laboratory testing including grain size distribution and Atterberg limits and hand penetrometer.

The ground surface elevations, station and offset at the test boring locations were taken from the boring survey plan prepared by CEC personnel.

IV. FINDINGS

The borings exhibited 6 to 7 inches of asphalt over 8 to 9 inches of base course at the surface. Below the surface cover, the borings exhibited cohesive soils described as sandy silt (A-4a) or silt and clay (A-6a) soils and granular soils described as gravel and/or stone fragments with sand and silt (A-2-4) extending downwards to a depth of 8.0 feet. These soils exhibited standard penetration N_{60} values ranging from 10 to 51 blows per foot (bpf), with natural moisture content values ranging from 7 to 18 percent.

Below the near surface soils, the borings exhibited both granular and cohesive soils described as gravel and/or stone fragments with sand (A-1-b), coarse and fine sand (A-3a), sandy silt (A-4a) or silt and clay (A-6a) soils extending downwards to the drilled depths. The cohesive A-4a and A-6a soils encountered below 17.5 feet within this layer were further classified as glacial till deposits. These soils exhibited N_{60} values ranging from 7 bpf to 50 blows for 3 inches of penetration, with moisture content values ranging from 7 to 32 percent.

Groundwater was encountered during drilling at depths ranging from 17.0 to 20.0 feet. Upon completion of drilling, groundwater levels were measured at depths ranging from 7.8 to 17.4 feet.

V. ANALYSES AND RECOMMENDATIONS

A. Creek Bed Material

For the purpose of scour analysis, the D_{50} and type of creek bed materials encountered are shown in Table 1 below.

Table 1. D_{50} Values

Boring No.	Sample No.	Depth (feet)	D_{50} (mm)	Soil Type
B-001-0-16	SS-5	11.0-12.5	0.047	A-4a
	SS-6	12.5-14.0	0.046	A-4a
	SS-7	14.0-15.5	0.127	A-4a
B-002-0-16	SS-6	13.5-15.0	0.176	A-3a

B. Foundation Support

It is understood that the replacement structure will be 36 feet (clear span) by 9 feet (rise) conduit type A, precast reinforced concrete arch sections, supported on spread footings. It is also understood that the foundations for the proposed structure will be constructed about 12.9 to 14.4 feet below the existing roadway grade (Foundation Elevation = 702.42 feet). Medium dense granular deposits or hard cohesive soils were encountered in the test borings at the anticipated foundation level. These soils are considered suitable to support the foundations for the proposed structure.

Spread foundations may be proportioned using the bearing resistance values provided in the Table 2 below. The calculations are provided in Appendix D.

Table 2. Bearing Resistance

Boring Number	Nominal Bearing Resistance (q_n), Ksf (Strength Limit State)	Presumptive Bearing Resistance (q_r), Ksf (Service Limit State)
B-001-0-16	16.5	8.0
B-002-0-16	12.5	5.0

The applicable resistance factors for the bearing resistance and sliding are provided in Table 3 below. These values are obtained from AASHTO Table 10.5.5.2.2-1 and section 11.5.7.

Table 3. Resistance Factors

Boring Number	Resistance Factors		
	Bearing Resistance		Sliding
	Strength Limit State	Service Limit State	
B-001-0-16	0.50	1.0	0.85
B-002-0-16	0.45	1.0	0.80

Surface water and groundwater seepage should be expected during excavation and construction of the spread foundations. In such an event, the groundwater level will need to temporarily lowered to facilitate construction of the foundations. Additionally, cofferdams may need to be constructed to facilitate excavation and construction of the foundations. A mud mat consisting of a few inches of lean concrete, may be needed to provide a relatively dry surface for setting reinforcing steel and placing concrete.

For sliding and lateral earth pressure calculations for the proposed structure and any headwalls, wingwalls or temporary shoring, an equivalent friction angle of 30 degrees, and a total unit weight value of 125 pcf may be used.

C. General Construction and Earthwork

1. Site preparation and earthwork should be performed in accordance with the ODOT Construction and Material Specifications.
2. Embankment side slopes should be seeded and vegetation growth permitted to limit erosion, sloughing and slope failure.
3. Temporary excavations in excess of 4 feet in depth should be sloped or shored according to OSHA requirements.

VI. CHANGED CONDITIONS

The evaluations, conclusions, and recommendations in this report are based on our interpretation of the field and laboratory data obtained during the exploration, our understanding of the project and our experience with similar sites and subsurface conditions using generally accepted geotechnical engineering practices. Although individual test borings are representative of the subsurface conditions at the boring locations on the dates drilled, they are not necessarily representative of the subsurface conditions between boring locations or subsurface conditions during other seasons of the year.



In the event that changes in the project are proposed, additional information becomes available, or if it is apparent that subsurface conditions are different from those provided in this report, CTL Engineering should be notified so that our recommendations can be modified, if required.

VII. TESTING AND OBSERVATION

During the design process, it is recommended that CTL Engineering work with the project designers to confirm that the geotechnical recommendations are properly incorporated into the final plans and specifications, and to assist with establishing criteria for the construction observation and testing.

CTL Engineering is not responsible for independent conclusions, opinions and recommendations made by others based on the data and recommendations provided in this report. It is recommended that CTL be retained to provide construction quality control services on this project. If CTL Engineering is not retained for these services, CTL shall assume no responsibility for compliance with the design concepts or recommendations provided.

VIII. CLOSING

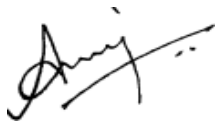
This report has been prepared for the exclusive use by the client for use only on this project. Our services have been performed in accordance with generally accepted Geotechnical Engineering principles and practices. No warranty is either expressed or implied.

CTL Engineering's assignment does not include, nor does this geotechnical report address the environmental aspects of this particular site.

Specific design and construction recommendations have been provided in this report. Therefore, the report should be used in its entirety.

Respectfully Submitted,

CTL ENGINEERING, INC.



Anuj Choudhari, E.I.
Staff Engineer



Joe Grani, P.E.
Project Engineer

APPENDIX A
STRUCTURE FOUNDATION EXPLORATION SHEETS



PROJECT DESCRIPTION

REPLACEMENT OF THE EXISTING FRA - T266 - 3.84 (BORROR ROAD) STRUCTURE OVER PATZER DITCH IN JACKSON TOWNSHIP, FRANKLIN COUNTY, OHIO. THE REPLACEMENT STRUCTURE WILL BE 36 FEET (CLEAR SPAN) BY 9 FEET (RISE) CONDUIT TYPE A, PRECAST REINFORCED CONCRETE ARCH SECTIONS, SUPPORTED ON SPREAD FOOTINGS.

HISTORIC RECORDS

HISTORIC GEOTECHNICAL RECORDS WERE SEARCHED FOR ON THE ODOT GEOMS WEBSITE. NO HISTORIC GEOTECHNICAL RECORDS WERE FOUND IN THE IMMEDIATE VICINITY OF THE PROPOSED BRIDGE.

GEOLOGY

ACCORDING TO THE OHIO DEPARTMENT OF NATURAL RESOURCES, PHYSIOGRAPHIC REGIONS OF OHIO, THIS SITE LIES ON THE COLUMBUS LOWLAND REGION OF SOUTHERN OHIO LOAMY TILL PLAIN.

ACCORDING TO THE BEDROCK GEOLOGY MAP OF OHIO (2006), THE BEDROCK BELOW THE SITE CONSISTS OF DEVONIAN AGE OHIO SHALE. NO BEDROCK WAS ENCOUNTERED WITHIN THE DRILLED DEPTHS OF THE TEST BORINGS.

RECONNAISSANCE

THE MOST RECENT SITE VISIT WAS PERFORMED ON DECEMBER 19, 2016. THE EXISTING PAVEMENT EXHIBITED SOME TRANSVERSE AND LONGITUDINAL CRACKS.

SUBSURFACE EXPLORATION

TWO (2) TEST BORINGS WERE DRILLED FOR THIS PROJECT.

THE BORINGS WERE DRILLED WITH A TRACK MOUNTED DRILL RIG USING 3-1/4 INCH I.D. HOLLOW-STEM AUGERS. DISTURBED SOIL SAMPLES WERE OBTAINED IN THE TEST BORINGS IN ACCORDANCE WITH THE STANDARD PENETRATION TEST (AASHTO T206) CONTINUOUSLY AND AT 2.5-FOOT TO 5.0-FOOT INTERVALS THROUGH THE SOIL USING AN AUTOMATIC HAMMER SYSTEM. THE HAMMER WAS CALIBRATED ON JULY 1, 2015 AND HAD A DRILL ROD ENERGY RATIO OF 81.9%.

CONTINUOUS SPLIT-SPOON SOIL SAMPLING WAS PERFORMED IN TEST BORING B-001-0-17 FOR A 7.5-FOOT INTERVAL BELOW THE APPROXIMATE STREAM BED ELEVATION. D50 VALUES WHICH HAVE BEEN CALCULATED FOR THE SCOUR ANALYSIS ARE PRESENTED ON THIS PAGE.

EXPLORATION FINDINGS

THE BORINGS EXHIBITED 6 TO 7 INCHES OF ASPHALT OVER 8 TO 9 INCHES OF BASE COURSE AT THE SURFACE

BELOW THE SURFACE COVER, THE BORINGS EXHIBITED COHESIVE SOILS DESCRIBED AS SANDY SILT (A-4a) OR SILT AND CLAY (A-6a) SOILS AND GRANULAR SOILS DESCRIBED AS GRAVEL AND/OR STONE FRAGMENTS WITH SAND AND SILT (A-2-4) EXTENDING DOWNWARDS TO A DEPTH OF 8.0 FEET.

BELOW THE NEAR SURFACE SOILS, THE BORINGS EXHIBITED BOTH GRANULAR AND COHESIVE SOILS DESCRIBED AS GRAVEL AND/OR STONE FRAGMENTS WITH SAND (A-1-b), COARSE AND FINE SAND (A-3a), SANDY SILT (A-4a) OR SILT AND CLAY (A-6a) SOILS EXTENDING DOWNWARDS TO THE DRILLED DEPTHS. THE COHESIVE A-4a AND A-6a SOILS ENCOUNTERED BELOW 17.5 FEET WITHIN THIS LAYER WERE FURTHER CLASSIFIED AS GLACIAL TILL DEPOSITS.

GROUND WATER WAS ENCOUNTERED DURING DRILLING AT DEPTHS RANGING FROM 17.0 TO 20.0 FEET (ELEVATIONS 698.3 FEET AND 696.8 FEET, RESPECTIVELY). UPON COMPLETION OF DRILLING, GROUNDWATER LEVELS WERE MEASURED AT DEPTHS RANGING FROM 7.8 TO 17.4 FEET (ELEVATIONS 707.5 FEET AND 699.4 FEET, RESPECTIVELY).

SPECIFICATIONS

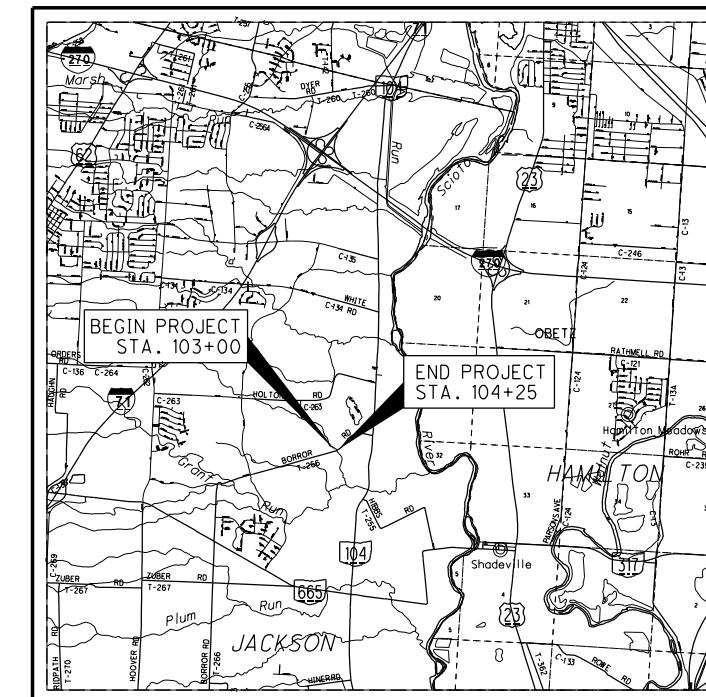
THIS GEOTECHNICAL EXPLORATION WAS PERFORMED IN ACCORDANCE WITH THE STATE OF OHIO, DEPARTMENT OF TRANSPORTATION, OFFICE OF GEOTECHNICAL ENGINEERING, SPECIFICATIONS FOR GEOTECHNICAL EXPLORATIONS, DATED JULY 2016.

AVAILABLE INFORMATION

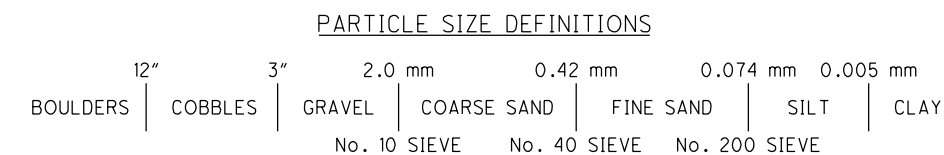
ALL AVAILABLE SOIL INFORMATION THAT CAN BE CONVENIENTLY SHOWN ON THE SOIL PROFILE SHEETS HAS BEEN SO REPORTED. ADDITIONAL SUBSURFACE EXPLORATIONS MAY HAVE BEEN MADE TO STUDY SOME SPECIAL ASPECT OF THE PROJECT. COPIES OF THIS DATA, IF ANY, MAY BE INSPECTED IN THE FRANKLIN COUNTY ENGINEERS OFFICE.

LEGEND		ODOT CLASS	CLASSIFIED MECH./VISUAL	
DESCRIPTION				
	GRAVEL AND/OR STONE FRAGMENTS WITH SAND	A-1-b	1	4
	GRAVEL AND/OR STONE FRAGMENTS W/SAND AND SILT	A-2-4	1	0
	COARSE AND FINE SAND	A-3a	2	8
	SANDY SILT	A-4a	4	9
	SILT AND CLAY	A-6a	2	5
	TOTAL		10	26
	PAVEMENT OR BASE = X = APPROXIMATE THICKNESS	VISUAL		
	BORING LOCATION - PLAN VIEW.			
<i>WC</i>	INDICATES WATER CONTENT IN PERCENT.			
<i>N₆₀</i>	INDICATES STANDARD PENETRATION RESISTANCE NORMALIZED TO 60% DRILL ROD ENERGY RATIO.			
<i>W</i>	INDICATES FREE WATER ELEVATION.			
	INDICATES A NON-PLASTIC MATERIAL WITH A MOISTURE CONTENT GREATER THAN 25 % OR GREATER THAN 19 % WITH A WET APPEARANCE.			
<i>SS</i>	INDICATES A SPLIT SPOON SAMPLE.			
<i>NP</i>	INDICATES A NON-PLASTIC SAMPLE.			

D ₅₀ VALUES			
BORING NO.	SAMPLE NO.	ELEVATION	D ₅₀ VALUE
B-001-0-16	SS-5	705.8' - 704.3'	0.047 mm
	SS-6	704.3' - 702.8'	0.046 mm
	SS-7	702.8' - 701.3'	0.127 mm
B-002-0-16	SS-6	701.8' - 700.3'	0.176 mm



LOCATION MAP



RECON. - LH 12/19/2016
 DRILLING - CTL ENGINEERING, INC. 12/19/2016 - 12/20/2016
 DRAWN - BRU 05/31/17
 REVIEWED - JG 05/31/17

j:\dept5\16 Projects\16050169COL-CEC-Borrer Rd Bridge\Design\Sachina\From Sachina\17.06.02 16050169COL_ODOT\ZC001.dgn Sheet 6/8/2017 2:49:43 PM achoudhari

CTL ENGINEERING, INC.
 2860 FISHER ROAD
 COLUMBUS, OHIO 43204
 PHONE: (614) 276-8123 FAX: (614) 276-6377

PID NO. -

STRUCTURE FOUNDATION EXPLORATION
BR. NO. FRA-T266-3.84 OVER PATZER DITCH

FRA-T266-3.84

1 / 5

PROJECT: FRA-T266-3.84	DRILLING FIRM / OPERATOR: CTL / LH	DRILL RIG: MOBILE B-57/#487	STATION / OFFSET: 103+91, 6' LT.	EXPLORATION ID B-002-0-16
TYPE: STRUCTURE FOUNDATION	SAMPLING FIRM / LOGGER: CTL / LH	HAMMER: MOBILE AUTOMATIC	ALIGNMENT:	PAGE 1 OF 2
PID: SFN: 2531593	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 7/1/15	ELEVATION: 715.3 (MSL) EOB: 65.0 ft.	
START: 12/19/16 END: 12/19/16	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	COORD: 673209.5864 N, 1818134.7245 E	

MATERIAL DESCRIPTION AND NOTES	ELEV.	DEPTHS	SPT/RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			ODOT CLASS (GI)	BACK FILL	
								GR	CS	FS	SI	CL	LL	PL	PI			WC
Asphalt (6")	715.3																	
Base course (9")	714.0	1																
VERY STIFF, BROWN, SILT AND CLAY, SOME SAND, TRACE GRAVEL, POSSIBLE FILL, DAMP @3.5'; STIFF, CONTAINS STONE FRAGMENTS		2	4	5	12	67	SS-1	2.50	8	11	22	35	24	33	19	14	18	A-6a (6)
		3																
		4	4	5	12	50	SS-2	2.00	-	-	-	-	-	-	-	-	13	A-6a (V)
		5																
LOOSE, BROWN, COARSE AND FINE SAND, SOME SILT, LITTLE GRAVEL, TRACE CLAY, MOIST @11.0'; MEDIUM DENSE	707.3	6	3	4	51	56	SS-3	2.00	-	-	-	-	-	-	-	-	13	A-6a (V)
		7																
		8	1	2	7	67	SS-4	-	-	-	-	-	-	-	-	-	16	A-3a (V)
		9																
@16.0'; WET		10	3	3	11	50	SS-5	-	-	-	-	-	-	-	-	-	10	A-3a (V)
		11																
		12	7	6	15	78	SS-6	-	11	20	38	22	9	NP	NP	NP	15	A-3a (0)
		13																
MEDIUM DENSE, BROWN, GRAVEL AND/OR STONE FRAGMENTS WITH SAND, LITTLE SILT, TRACE CLAY, WET @33.5'; DENSE, TRACE CLAY	697.3	14	4	7	22	72	SS-7	-	-	-	-	-	-	-	-	-	17	A-3a (V)
		15																
		16	4	9	26	94	SS-8	-	-	-	-	-	-	-	-	-	16	A-1-b (V)
		17																
@36.0'; HEAVY COBBLES		18	4	7	22	83	SS-9	-	-	-	-	-	-	-	-	-	18	A-1-b (V)
		19																
		20	5	6	22	100	SS-10	-	-	-	-	-	-	-	-	-	32	A-1-b (V)
		21																
HARD, BROWNISH GRAY, SILT AND CLAY, LITTLE SAND, TRACE GRAVEL, CONTAINS COBBLES AND STONE FRAGMENTS, TILL, DAMP @58.5'; VERY STIFF, LITTLE CLAY	677.8	22	4	6	19	100	SS-11	-	31	28	19	17	5	NP	NP	NP	17	A-1-b (0)
		23																
		24	9	13	44	100	SS-12	-	-	-	-	-	-	-	-	-	13	A-1-b (V)
		25																
HARD, GRAY, SANDY SILT, SOME CLAY, TRACE GRAVEL, CONTAINS COBBLES AND STONE FRAGMENTS, TILL, DAMP @58.5'; VERY STIFF, LITTLE CLAY	663.3	26	24	26	85	78	SS-13	4.50	-	-	-	-	-	-	-	-	9	A-6a (V)
		27																
		28	13	22	85	61	SS-14	4.50	-	-	-	-	-	-	-	-	9	A-6a (V)
		29																
		30	21	36	117	72	SS-15	4.50	-	-	-	-	-	-	-	-	8	A-6a (V)
		31																
		32	5	21	74	89	SS-16	4.50	-	-	-	-	-	-	-	-	9	A-4a (V)
		33																
	34	41	50/3"	-	89	SS-17	2.50	-	-	-	-	-	-	-	-	10	A-4a (V)	

STANDARD ODOT SOIL BORING LOG (11 X 17) - OH DOT.GDT - 5/30/17 10:56 - J:\DEPT\1516 PROJECTS\16050169COL-CEC-BORROR RD BRIDGE\REPORTS\LOGS\16050169COL.GPJ

PID: _____	SFN: 2531593	PROJECT: FRA-T266-3.84	STATION / OFFSET: 103+91, 6' LT.	START: 12/19/16	END: 12/19/16	PG 2 OF 2	B-002-0-16											
MATERIAL DESCRIPTION AND NOTES		ELEV.	DEPTHS	SPT/RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			ODOT CLASS (GI)	BACK FILL
HARD, GRAY, SANDY SILT, SOME CLAY, TRACE GRAVEL, CONTAINS COBBLES AND STONE FRAGMENTS, TILL, DAMP (continued)		655.3	61						GR	CS	FS	SI	CL	LL	PL	PI	WC	
			62															
@63.5'; HARD, SOME CLAY			63															
			64	31	-	100	SS-18	4.50	-	-	-	-	-	-	-	-	7	A-4a (V)
		650.3	65															
			EOB															

STANDARD ODOT SOIL BORING LOG (11 X 17) - OH DOT.GDT - 5/30/17 10:56 - J:\DEPT\1516 PROJECTS\16050169COL-CEC-BORROR RD BRIDGE\REPORTS\LOGS\16050169COL.GPJ

NOTES: CAVED AT 17.3'
 ABANDONMENT METHODS, MATERIALS, QUANTITIES: NOT RECORDED

APPENDIX B
TEST BORING RECORDS



SOIL DESCRIPTION

Descriptors for soil consistency used in this report are based upon the Standard Penetration Test (SPT), ASTM D 1587, with the penetration (N) values corrected to N_{60} , based upon the efficiency of the SPT Hammer used for the soil sampling.

Descriptors for both non-cohesive and cohesive soils are presented below, with the corresponding range of corrected penetration values.

<u>NON-COHESIVE SOIL DESCRIPTION</u>	<u>CORRECTED PENETRATION VALUES BLOWS PER FOOT (BPF)</u>
Very Loose.....	0 – 4
Loose.....	5 – 10
Medium Dense.....	11- 30
Dense.....	31 – 50
Very Dense.....	Over 50

<u>COHESIVE SOIL DESCRIPTION</u>	<u>CORRECTED PENETRATION VALUES BLOWS PER FOOT (BPF)</u>
Very Soft.....	0 – 1
Soft.....	2 – 4
Medium Stiff.....	5 – 8
Stiff.....	9 – 15
Very Stiff.....	16 –30
Hard.....	Over 30

Moisture term descriptors for both non-cohesive and cohesive soils are presented below.

<u>NON-COHESIVE SOIL DESCRIPTION</u>	<u>MOISTURE TERMS</u>	<u>COHESIVE SOIL DESCRIPTION</u>
Powdery.....	Dry.....	Powdery
Some Moisture.....	Damp.....	Below Plastic Limit
Damp to the Touch.....	Moist.....	Above Plastic, Below Liquid Limit
Free Water.....	Wet.....	Above Liquid Limit



STANDARD ODOT SOIL BORING LOG (8.5 X 11) - OH DOT.GDT - 6/8/17 14:36 - J:\DEPT516 PROJECTS\16050169COL-CEC-BORROR RD BRIDGE\REPORTS\LOGS\16050169COL.GPJ

PID: _____		SFN: 2531593		PROJECT: FRA-T266-3.84		STATION / OFFSET: 103+40, 7' RT.		START: 12/20/16		END: 12/20/16		PG 2 OF 2		B-001-0-16					
MATERIAL DESCRIPTION AND NOTES		ELEV. 686.8	DEPTHS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL
									GR	CS	FS	SI	CL	LL	PL	PI			
MEDIUM DENSE, BROWN, COARSE AND FINE SAND , SOME GRAVEL, LITTLE SILT, TRACE CLAY, WET (continued)																			
@33.5'; VERY DENSE, DAMP			31 32 33 34 35	25 32 29	83	94	SS-13	-	25	16	36	14	9	NP	NP	NP	10	A-3a (0)	
@38.5'; CONTAINS COBBLES, WET			36 37 38 39 40 41 42 43	50/3"	-	100	SS-14	-	-	-	-	-	-	-	-	-	12	A-3a (V)	
@43.5'; TRACE SILT, CLAY, DAMP			44 45 46 47 48 49 50 51	50/4"	-	100	SS-15	-	-	-	-	-	-	-	-	-	11	A-3a (V)	
HARD, GRAY, SILT AND CLAY , SOME SAND, TRACE GRAVEL, TILL, DAMP		671.8	52 53 54 55 56 57 58	9 25 43	93	89	SS-16	4.50	8	10	24	33	25	25	14	11	9	A-6a (5)	
HARD, GRAY, SANDY SILT , SOME CLAY, CONTAINS STONE FRAGMENTS, TILL, DAMP		664.8	59 60	5 30 50/3"	-	100	SS-17	4.50	-	-	-	-	-	-	-	-	7	A-4a (V)	
		656.8	EOB	50	-	100	SS-18	4.00	-	-	-	-	-	-	-	-	12	A-4a (V)	

NOTES: CAVED AT 24.0'
 ABANDONMENT METHODS, MATERIALS, QUANTITIES: NOT RECORDED

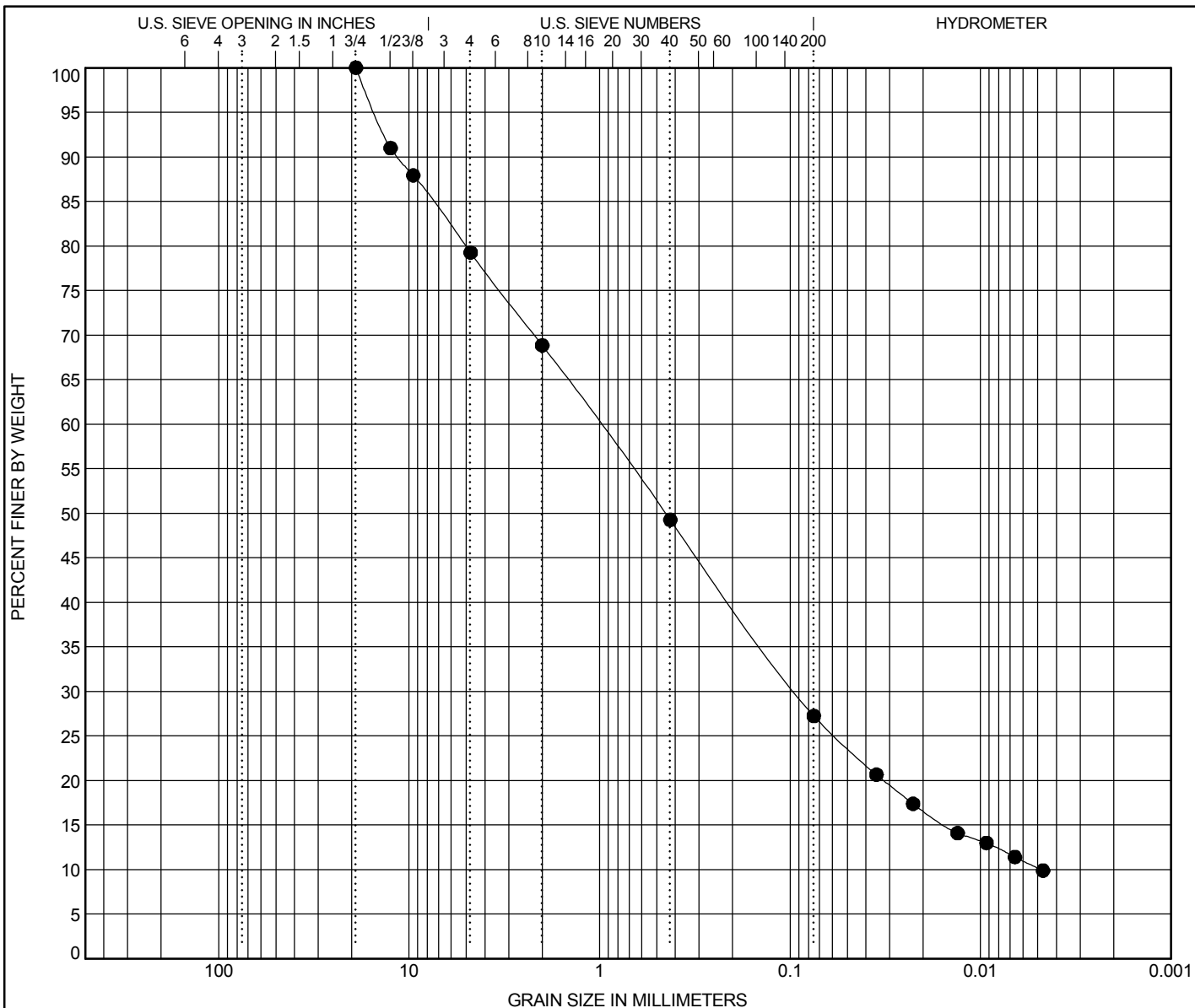
STANDARD ODOT SOIL BORING LOG (8.5 X 11) - OH DOT.GDT - 6/8/17 14:36 - J:\DEPT5\16 PROJECTS\16050169COL-CEC-BORROR RD BRIDGE\REPORTS\LOGS\16050169COL.GPJ

PID: _____		SFN: 2531593		PROJECT: FRA-T266-3.84		STATION / OFFSET: 103+91, 6' LT.		START: 12/19/16		END: 12/19/16		PG 3 OF 3		B-002-0-16									
MATERIAL DESCRIPTION AND NOTES				ELEV. 653.1	DEPTHS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL		
											GR	CS	FS	SI	CL	LL	PL	PI					
HARD, GRAY, SANDY SILT , SOME CLAY, TRACE GRAVEL, CONTAINS COBBLES AND STONE FRAGMENTS, TILL, DAMP (continued) @63.5'; HARD, SOME CLAY				650.3	63																		
					64	31 50/3"	-	100															
					EOB	65			SS-18	4.50	-	-	-	-	-	-	-	-		7	A-4a (V)		
<p>NOTES: CAVED AT 17.3'</p> <p>ABANDONMENT METHODS, MATERIALS, QUANTITIES: NOT RECORDED</p>																							

APPENDIX C
LABORATORY TEST SHEETS



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COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification	MC	LL	PL	PI	Cc	Cu
B-001-0-16	1.5	A-2-4(0)	11	24	17	7	1.81	205.72

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
B-001-0-16	1.5	19	0.995	0.451	0.093	0.005	31	20	22	17	10

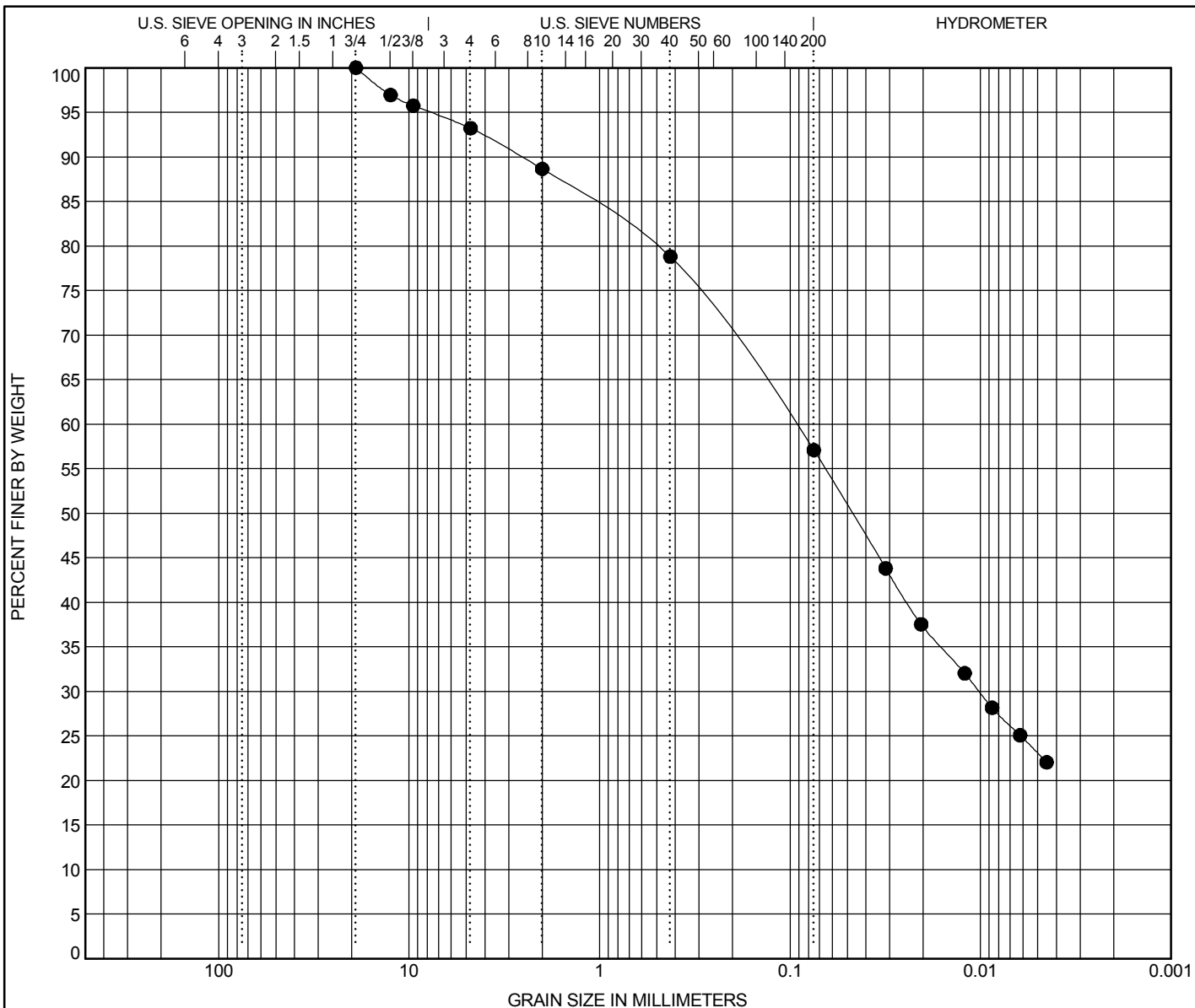


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 Columbus, Ohio 43204
 Telephone: 614-276-8123
 Fax: 614-276-6377

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COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification					MC	LL	PL	PI	Cc	Cu
B-001-0-16	11.0	A-4a(4)					13	26	16	10		

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
B-001-0-16	11.0	19	0.095	0.047	0.01		11	10	22	34	23

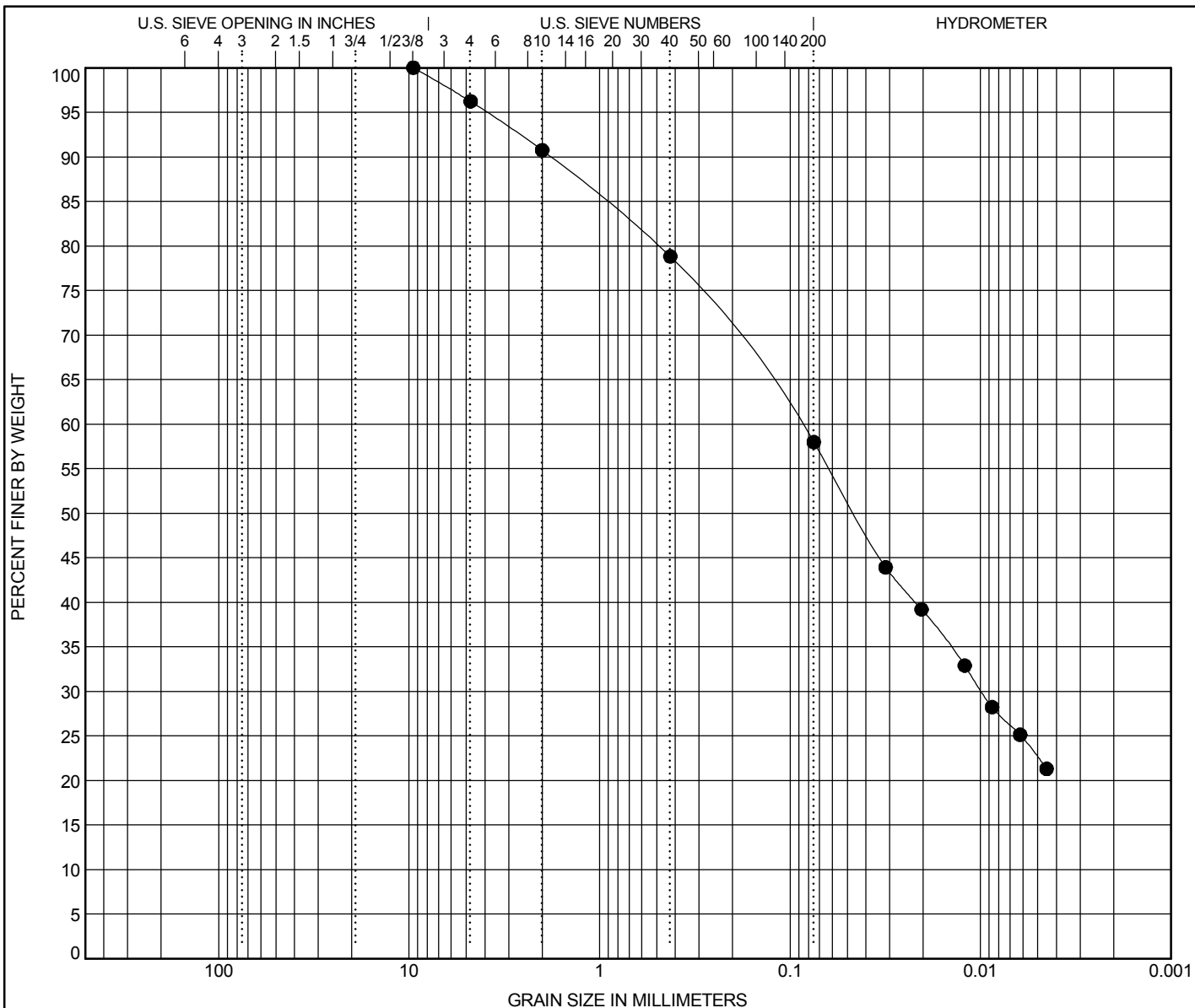


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COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification	MC	LL	PL	PI	Cc	Cu
B-001-0-16	12.5	A-4a(5)	11	24	15	9		

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
B-001-0-16	12.5	9.5	0.089	0.046	0.01		9	12	21	35	23

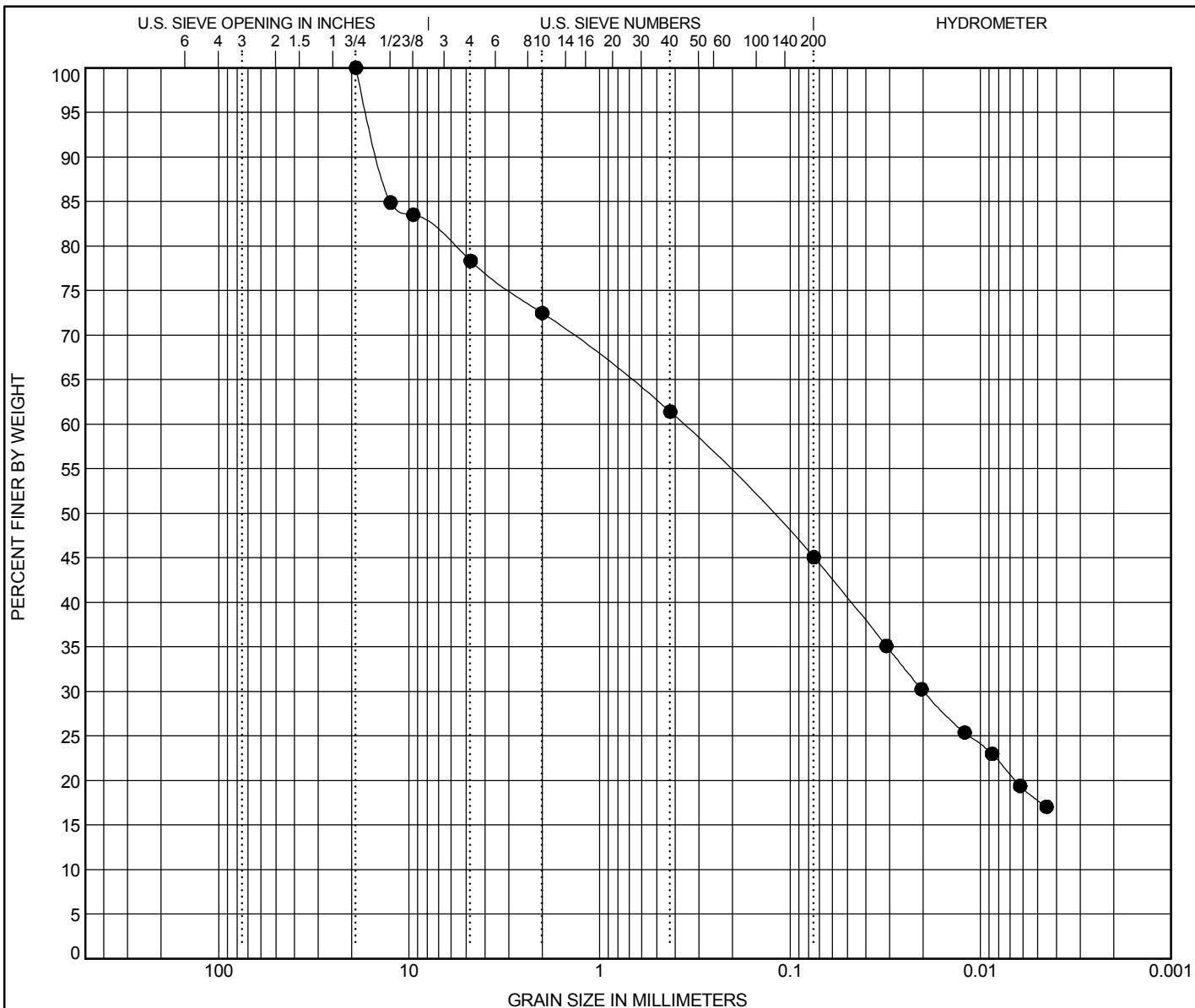


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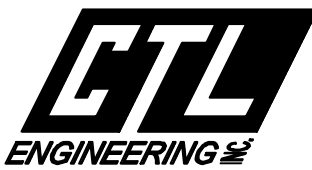
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COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification					MC	LL	PL	PI	Cc	Cu
B-001-0-16	14.0	A-4a(2)					10	21	13	8		

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
B-001-0-16	14.0	19	0.367	0.127	0.02		28	11	16	27	18

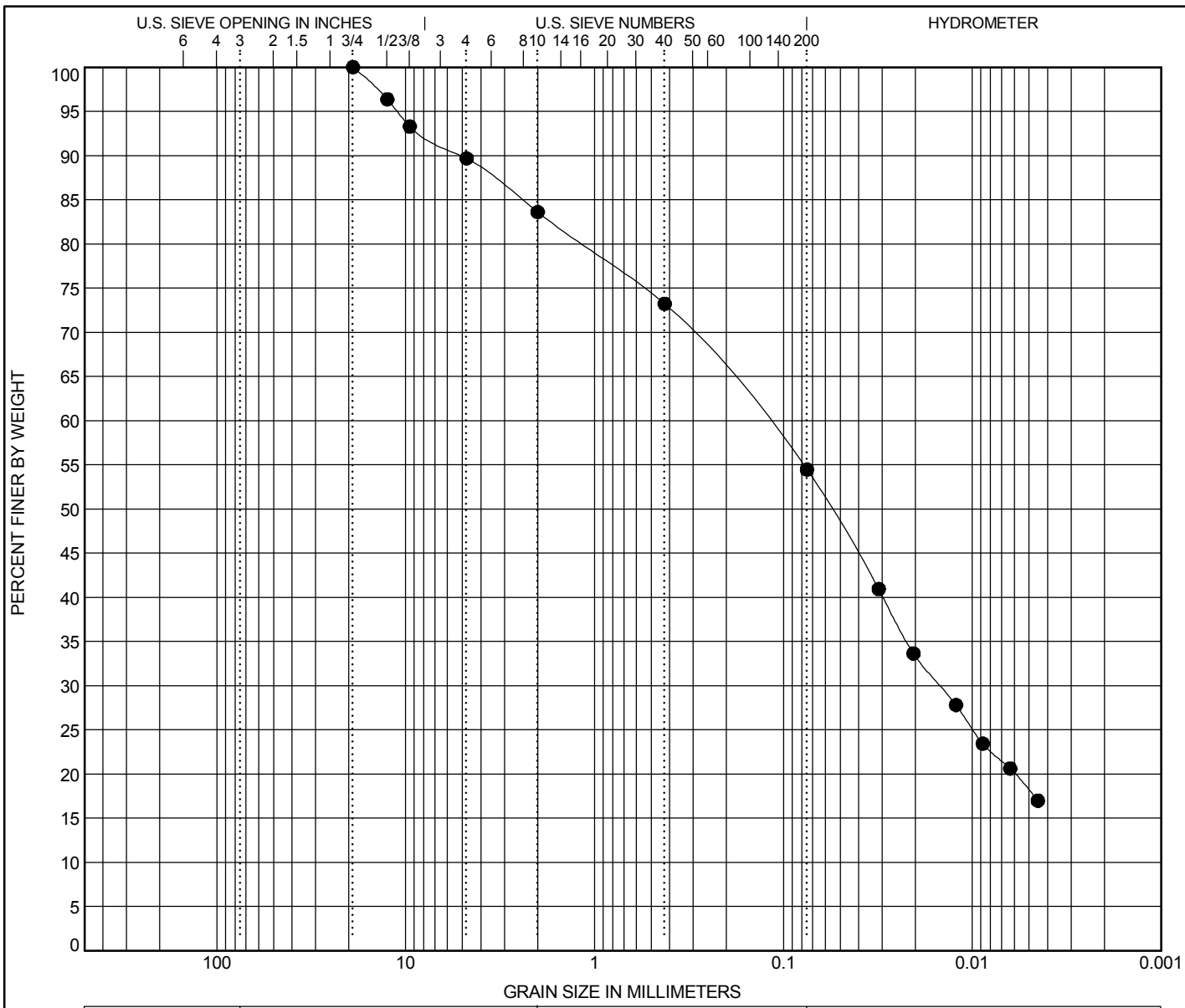


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COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification	MC	LL	PL	PI	Cc	Cu
B-001-0-16	18.0	A-4a(4)	10	21	14	7		

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
B-001-0-16	18.0	19	0.125	0.056	0.015		17	10	19	36	18

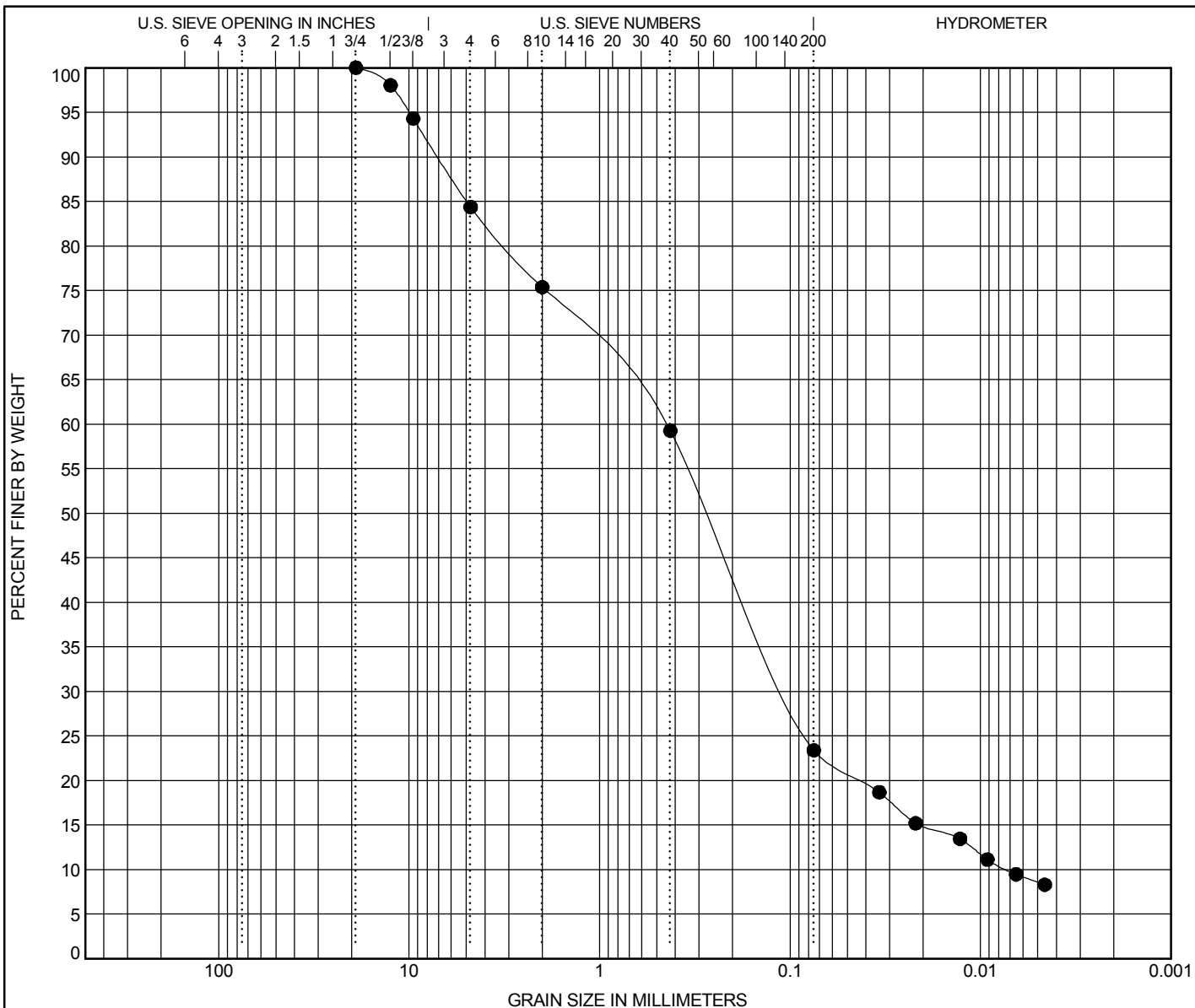


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COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification	MC	LL	PL	PI	Cc	Cu
B-001-0-16	33.5	A-3a(0)	10	NP	NP	NP	3.21	62.53

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
B-001-0-16	33.5	19	0.456	0.272	0.103	0.007	25	16	36	14	9

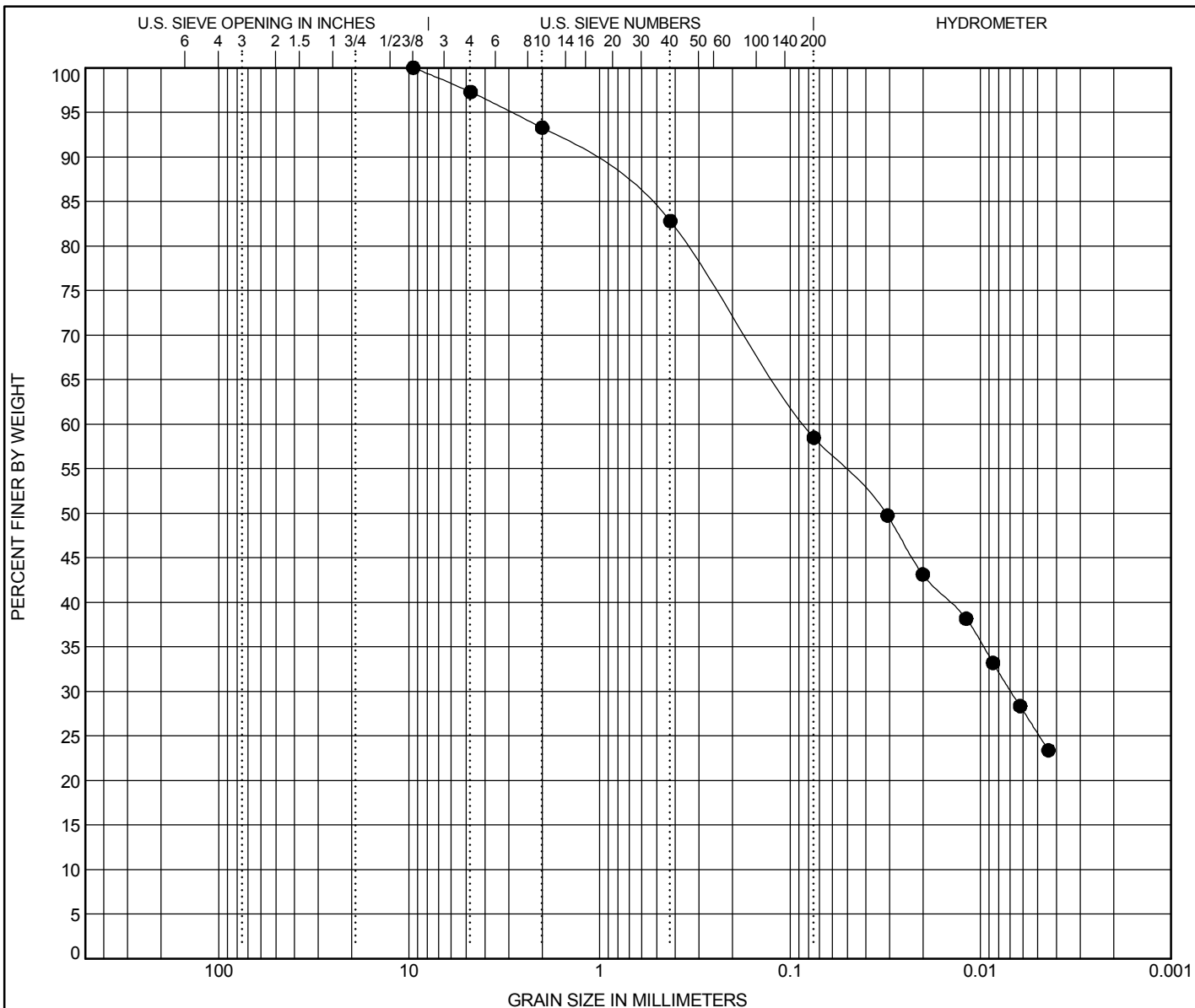


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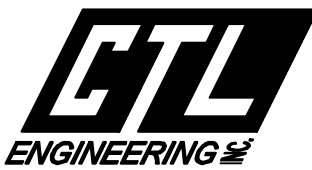
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COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification					MC	LL	PL	PI	Cc	Cu
B-001-0-16	48.5	A-6a(5)					9	25	14	11		

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
B-001-0-16	48.5	9.5	0.084	0.032	0.007		8	10	24	33	25

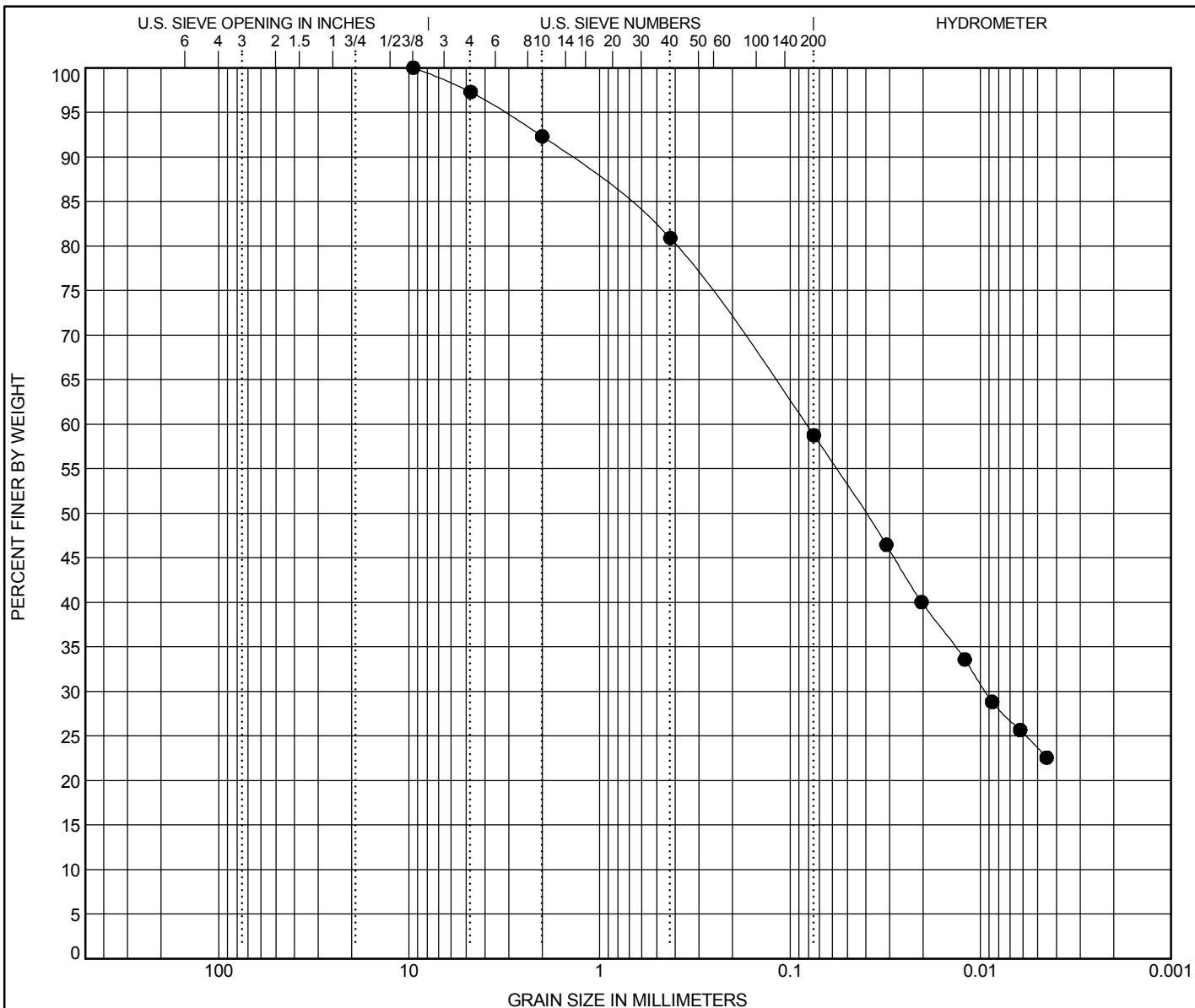


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COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification	MC	LL	PL	PI	Cc	Cu
B-002-0-16	1.5	A-6a(6)	18	33	19	14		

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
B-002-0-16	1.5	9.5	0.083	0.04	0.009		8	11	22	35	24

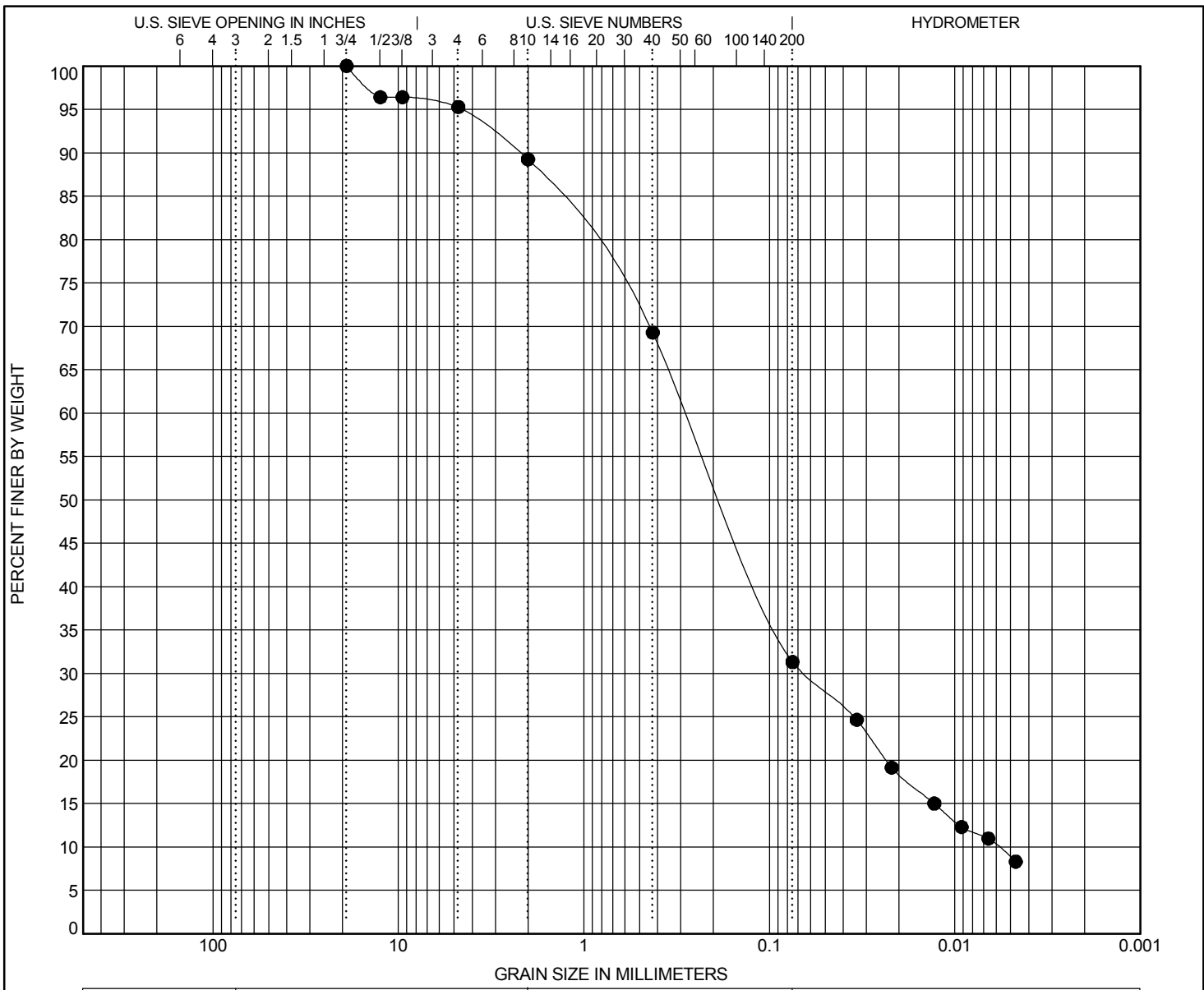


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COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification	MC	LL	PL	PI	Cc	Cu
B-002-0-16	13.5	A-3a(0)	15	NP	NP	NP	2.54	47.61

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
B-002-0-16	13.5	19	0.278	0.176	0.064	0.006	11	20	38	22	9

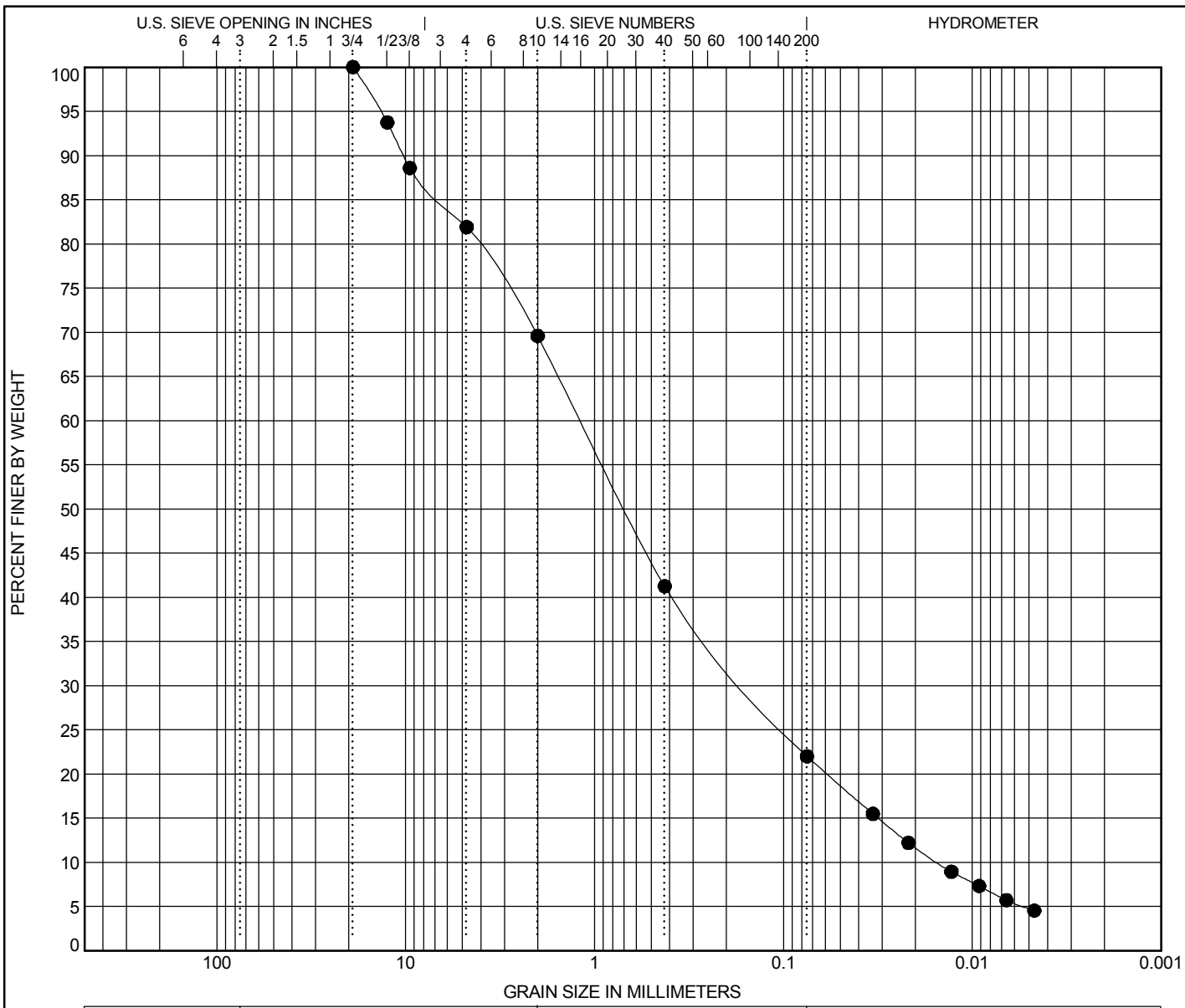


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COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification					MC	LL	PL	PI	Cc	Cu
B-002-0-16	28.5	A-1-b(0)					17	NP	NP	NP	1.31	77.23

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
B-002-0-16	28.5	19	1.185	0.686	0.154	0.015	31	28	19	17	5



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GRAIN SIZE DISTRIBUTION

Project: FRA-T266-3.84
 Location: FRA COUNTY
 CTL Project Number:

APPENDIX D
BEARING RESISTANCE CALCULATIONS



Project
Project No.
Boring No.

Borrer Road Bridge over Patzer Ditch
16050169COL
B-001-0-16

Bearing Resistance- Strength Limit State

Cohesion, c	3.0	ksf
Friction Angle, ϕ_b	0	Degrees
Footing Width, B	9.00	feet
Unit Wt. of Soil, γ	0.125	kcf
Footing Length, L_f	35	ft
Footing Embedment Depth, D_f	4.5	ft
GW Depth Below Footing, D_w	0	ft

Nom. Bearing Resistance, q_n 16.5 ksf $=c_i N_c s_c + \gamma D_f N_q s_q d_q C_{wq} + 0.5 \gamma B N_\gamma s_\gamma C_{w\gamma}$

Where

N_c	5.14	
N_q	1	Table 10.6.3.1.2a-1
N_γ	0	
s_c	1.05	$=1+(B/L_f)*(N_q/N_c)$; or $1+(B/5L_f)$ for $\phi = 0$
s_q	1.00	$=1+(B/L_f)*\tan\phi_i$; or 1.0 for $\phi = 0$ Table 10.6.3.1.2a-3
s_γ	1.00	$=1-0.4*(B/L_f)$; or 1.0 for $\phi = 0$
C_{wq}	0.50	Table 10.6.3.1.2a-2
$C_{w\gamma}$	0.50	
$1.5B+D_f$	18.00	ft For C_w Check
D_f/B	0.50	For d_q by Hansen 1970
d_q	1.00	Hansen 1970 or Table 10.6.3.1.2a-4
Fact. Bearing Resistance, q_r	8.2	ksf $=\phi_b * q_n$
Resistance Factor, ϕ_b	0.5	Table 10.5.5.2.2-1

Bearing Resistance- Service Limit State

Pres. Bearing Resistance, q_r	8.0	ksf Table C10.6.2.6.1-1
Resistance Factor, ϕ_r	1.0	Section 11.5.7

Project
Project No.
Boring No.

Borrer Road Bridge over Patzer Ditch
16050169COL
B-002-0-16

Bearing Resistance- Strength Limit State

Cohesion, c	0.0	ksf
Friction Angle, ϕ_b	30	Degrees
Footing Width, B	9.00	feet
Unit Wt. of Soil, γ	0.125	kcf
Footing Length, L_f	35	ft
Footing Embedment Depth, D_f	4.5	ft
GW Depth Below Footing, D_w	0	ft

Nom. Bearing Resistance, q_n 12.5 ksf $=c_i N_c s_c + \gamma D_f N_q s_q d_q C_{wq} + 0.5 \gamma B N_\gamma s_\gamma C_{w\gamma}$

Where

N_c	30.1	
N_q	18.4	Table 10.6.3.1.2a-1
N_γ	22.4	
s_c	1.16	$=1+(B/L_f)*(N_q/N_c)$; or $1+(B/5L_f)$ for $\phi = 0$
s_q	1.15	$=1+(B/L_f) \cdot \tan \phi_i$; or 1.0 for $\phi = 0$ Table 10.6.3.1.2a-3
s_γ	0.90	$=1-0.4*(B/L_f)$; or 1.0 for $\phi = 0$
C_{wq}	0.50	Table 10.6.3.1.2a-2
$C_{w\gamma}$	0.50	
$1.5B+D_f$	18.00	ft For C_w Check
D_f/B	0.50	For d_q by Hansen 1970
d_q	1.14	Hansen 1970 or Table 10.6.3.1.2a-4
Fact. Bearing Resistance, q_r	5.6	ksf $=\phi_b * q_n$
Resistance Factor, ϕ_b	0.45	Table 10.5.5.2.2-1

Bearing Resistance- Service Limit State

Pres. Bearing Resistance, q_r	5.0	ksf Table C10.6.2.6.1-1
Resistance Factor, ϕ_r	1.0	11.5.7