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AN EMPLOYEE OWNED COMPANY



Consulting Engineers • Testing • Inspection Services • Analytical Laboratories

Established 1927

June 8, 2017

Columbus Engineering Consultants, Inc. 870 Michigan Avenue Columbus, Ohio 43215

Attention: Mr. Tom Hedrick, P.E.

Reference: Structure Foundation Exploration – Draft

Borror Road (T-266) Bridge over Patzer Ditch Jackson Township, Franklin County, Ohio

CTL Project No. 16050169COL

Dear Mr. Hedrick:

CTL Engineering, Inc. has completed the Structure Foundation Exploration report for the above referenced structure. A pdf copy of the draft report is being submitted.

Thank you for the opportunity to work with you on this project. If you have any questions or need further information, please feel free to contact our office.

Respectfully Submitted

CTL ENGINEERING, INC.

Joe Grani, P.E. Project Engineer

Offices: Ohio, Indiana, West Virginia

STRUCTURE FOUNDATION EXPLORATION-DRAFT

BORROR ROAD (T-266) BRIDGE OVER PATZER DITCH JACKSON TOWNSHIP, FRANKLIN COUNTY, OHIO CTL PROJECT NO. 16050169COL

PREPARED FOR:

COLUMBUS ENGINEERING CONSULTANTS 870 MICHIGAN AVE. COLUMBUS, OHIO 43215

PREPARED BY:

CTL ENGINEERING, INC. 2860 FISHER ROAD COLUMBUS, OHIO 43204 Phone 614-276-8123 Fax 614-276-6377

June 8, 2017



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I. EXECUTIVE SUMMARY AND INTRODUCTION

The project involves the replacement of an existing bridge that carries Borror Road (T266) over Patzer Ditch in Jackson Township, Franklin County, Ohio. It is understood that the replacement structure will be a 36 feet (clear span) by 9 feet (rise) conduit type A, precast reinforced concrete arch sections, supported on spread footings.

Two test borings, identified as B-001-0-16 and B-002-0-16, were drilled for this Structure Foundation Exploration. The borings generally exhibited gravel and/or stone fragments with sand (A-1-b), gravel and/or stone fragments with sand and silt (A-2-4), coarse and fine sand (A-3a), sandy silt (A-4a) or silt and clay (A-6a) soils to the drilled depths. No bedrock was encountered within the drill depths.

It is understood that the foundations for the proposed arch bridge will be constructed about 12.9 to 14.4 feet below the existing roadway grade (Foundation Elevation = 702.42 feet). Medium dense granular deposits or hard cohesive soils were encountered in the test borings at the anticipated foundation level. These soils are considered suitable to support foundations for the proposed structure.

II. GEOLOGY AND OBSERVATIONS OF THE PROJECT

According to the Ohio Department of Natural Resources, *Physiographic Regions of Ohio*, the site lies on the Columbus Lowland region of Southern Ohio Loamy Till Plain.

According to Bedrock Geology Map of Ohio (2006), bedrock below the site consists of Devonian age shale. No bedrock was encountered in the drilled borings.

According to web based mapping from *United States Department of Agriculture, Natural Resources Conservation Service*, the project area contains soils primarily described as Miamian Silty Clay Loam, 12 to 18 percent slopes, eroded (MID2), Sloan Silt Loam, frequently flooded (So), and Kendallville Silt Loam, 2 to 6 percent slopes (KeB) soils. According to the *Soil Survey of Franklin County, Ohio*, these soils exhibit moderately high to high permeability.

According to the ODNR Website, no underground mines have been mapped below the structure. However, active sand, gravel and limestone surface mine operations are performed about 1 mile east of the structure.

According to the Ohio Karst Areas map prepared by the Ohio Department of Natural Resources (ODNR), the project site does not lie in a Probable Karst Area.

Historic geotechnical records were searched for on the ODOT GeoMS website. No historic geotechnical records were found for this site.



III. EXPLORATION

Two (2) structure test borings, designated as B-001-0-16 and B-002-0-16, were drilled to depths ranging from 60.0 to 65.0 feet below grade.

The borings were performed with a track mounted drill rig utilizing hollow stem augers (HSA) on December 19 and 20, 2016. Standard penetration tests were conducted using a 140-pound hammer falling 30 inches to drive a 2-inch O.D. split barrel sampler. The energy transfer ratio associated with the automatic SPT hammer was 81.9 percent. The hammer was calibrated in July 2015.

Soil samples obtained from the drilling operation were preserved in glass jars, visually classified in the field and laboratory, and tested for natural moisture content. Representative soil samples were subjected to laboratory testing including grain size distribution and Atterberg limits and hand penetrometer.

The ground surface elevations, station and offset at the test boring locations were taken from the boring survey plan prepared by CEC personnel.

IV. <u>FINDINGS</u>

The borings exhibited 6 to 7 inches of asphalt over 8 to 9 inches of base course at the surface. Below the surface cover, the borings exhibited cohesive soils described as sandy silt (A-4a) or silt and clay (A-6a) soils and granular soils described as gravel and/or stone fragments with sand and silt (A-2-4) extending downwards to a depth of 8.0 feet. These soils exhibited standard penetration N_{60} values ranging from 10 to 51 blows per foot (bpf), with natural moisture content values ranging from 7 to 18 percent.

Below the near surface soils, the borings exhibited both granular and cohesive soils described as gravel and/or stone fragments with sand (A-1-b), coarse and fine sand (A-3a), sandy silt (A-4a) or silt and clay (A-6a) soils extending downwards to the drilled depths. The cohesive A-4a and A-6a soils encountered below 17.5 feet within this layer were further classified as glacial till deposits. These soils exhibited N_{60} values ranging from 7 bpf to 50 blows for 3 inches of penetration, with moisture content values ranging from 7 to 32 percent.

Groundwater was encountered during drilling at depths ranging from 17.0 to 20.0 feet. Upon completion of drilling, groundwater levels were measured at depths ranging from 7.8 to 17.4 feet.



V. <u>ANALYSES AND RECOMMENDATIONS</u>

A. Creek Bed Material

For the purpose of scour analysis, the D_{50} and type of creek bed materials encountered are shown in Table 1 below.

Table 1. D₅₀ Values

Boring No.	Sample No.	Depth (feet)	D ₅₀ (mm)	Soil Type
	SS-5	11.0-12.5	0.047	A-4a
B-001-0-16	SS-6	12.5-14.0	0.046	A-4a
	SS-7	14.0-15.5	0.127	A-4a
B-002-0-16	SS-6	13.5-15.0	0.176	A-3a

B. <u>Foundation Support</u>

It is understood that the replacement structure will be 36 feet (clear span) by 9 feet (rise) conduit type A, precast reinforced concrete arch sections, supported on spread footings. It is also understood that the foundations for the proposed structure will be constructed about 12.9 to 14.4 feet below the existing roadway grade (Foundation Elevation = 702.42 feet). Medium dense granular deposits or hard cohesive soils were encountered in the test borings at the anticipated foundation level. These soils are considered suitable to support the foundations for the proposed structure.

Spread foundations may be proportioned using the bearing resistance values provided in the Table 2 below. The calculations are provided in Appendix D.

Table 2. Bearing Resistance

Boring Number	Nominal Bearing Resistance (qn), Ksf (Strength Limit State)	Presumptive Bearing Resistance (q _r), Ksf (Service Limit State)
B-001-0-16	16.5	8.0
B-002-0-16	12.5	5.0

The applicable resistance factors for the bearing resistance and sliding are provided in Table 3 below. These values are obtained from AASHTO Table 10.5.5.2.2-1 and section 11.5.7.



Table 3. Resistance Factors

		Resistance Factors					
Boring Number	Bearing R	Sliding					
	Strength Limit State	Service Limit State	Silding				
B-001-0-16	0.50	1.0	0.85				
B-002-0-16	0.45	0.45 1.0					

Surface water and groundwater seepage should be expected during excavation and construction of the spread foundations. In such an event, the groundwater level will need to temporarily lowered to facilitate construction of the foundations. Additionally, cofferdams may need to be constructed to facilitate excavation and construction of the foundations. A mud mat consisting of a few inches of lean concrete, may be needed to provide a relatively dry surface for setting reinforcing steel and placing concrete.

For sliding and lateral earth pressure calculations for the proposed structure and any headwalls, wingwalls or temporary shoring, an equivalent friction angle of 30 degrees, and a total unit weight value of 125 pcf may be used.

C. General Construction and Earthwork

- 1. Site preparation and earthwork should be performed in accordance with the ODOT Construction and Material Specifications.
- 2. Embankment side slopes should be seeded and vegetation growth permitted to limit erosion, sloughing and slope failure.
- 3. Temporary excavations in excess of 4 feet in depth should be sloped or shored according to OSHA requirements.

VI. CHANGED CONDITIONS

The evaluations, conclusions, and recommendations in this report are based on our interpretation of the field and laboratory data obtained during the exploration, our understanding of the project and our experience with similar sites and subsurface conditions using generally accepted geotechnical engineering practices. Although individual test borings are representative of the subsurface conditions at the boring locations on the dates drilled, they are not necessarily representative of the subsurface conditions between boring locations or subsurface conditions during other seasons of the year.



In the event that changes in the project are proposed, additional information becomes available, or if it is apparent that subsurface conditions are different from those provided in this report, CTL Engineering should be notified so that our recommendations can modified, if required.

VII. TESTING AND OBSERVATION

During the design process, it is recommended that CTL Engineering work with the project designers to confirm that the geotechnical recommendations are properly incorporated into the final plans and specifications, and to assist with establishing criteria for the construction observation and testing.

CTL Engineering is not responsible for independent conclusions, opinions and recommendations made by others based on the data and recommendations provided in this report. It is recommended that CTL be retained to provide construction quality control services on this project. If CTL Engineering is not retained for these services, CTL shall assume no responsibility for compliance with the design concepts or recommendations provided.

VIII. <u>CLOSING</u>

This report has been prepared for the exclusive use by the client for use only on this project. Our services have been performed in accordance with generally accepted Geotechnical Engineering principles and practices. No warranty is either expressed or implied.

CTL Engineering's assignment does not include, nor does this geotechnical report address the environmental aspects of this particular site.

Specific design and construction recommendations have been provided in this report. Therefore, the report should be used in its entirety.

Respectfully Submitted,

CTL ENGINEERING, INC.

Anuj Choudhari, E.I.

Staff Engineer

Joe Grani, P.E. Project Engineer



APPENDIX A STRUCTURE FOUNDATION EXPLORATION SHEETS



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EXPLORATION PATZER DITC

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TRUCTURE NO. FRA-1

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PROJECT DESCRIPTION

REPLACEMENT OF THE EXISTING FRA - T266 - 3.84 (BORROR ROAD) STRUCTURE OVER PATZER DITCH IN JACKSON TOWNSHIP, FRANKLIN COUNTY, OHIO. THE REPLACEMENT STRUCTURE WILL BE 36 FEET (CLEAR SPAN) BY 9 FEET (RISE) CONDUIT TYPE A. PRECAST REINFORCED CONCRETE ARCH SECTIONS, SUPPORTED ON SPREAD FOOTINGS.

HISTORIC RECORDS

HISTORIC GEOTECHNICAL RECORDS WERE SEARCHED FOR ON THE ODOT GEOMS WEBSITE. NO HISTORIC GEOTECHNICAL RECORDS WERE FOUND IN THE IMMEDIATE VICINITY OF THE PROPOSED BRIDGE.

GEOLOGY

ACCORDING TO THE OHIO DEPARTMENT OF NATURAL RESOURCES, PHYSIOGRAPHIC REGIONS OF OHIO, THIS SITE LIES ON THE COLUMBUS LOWLAND REGION OF SOUTHERN OHIO LOAMY

ACCORDING TO THE BEDROCK GEOLOGY MAP OF OHIO (2006). THE BEDROCK BELOW THE SITE CONSISTS OF DEVONIAN AGE OHIO SHALE. NO BEDROCK WAS ENCOUNTERED WITHIN THE DRILLED DEPTHS OF THE TEST BORINGS.

RECONNAISSANCE

THE MOST RECENT SITE VISIT WAS PERFORMED ON DECEMBER 19, 2016. THE EXISTING PAVEMENT EXHIBITED SOME TRANSVERSE AND LONGITUDINAL CRACKS.

SUBSURFACE EXPLORATION

TWO (2) TEST BORINGS WERE DRILLED FOR THIS PROJECT.

THE BORINGS WERE DRILLED WITH A TRACK MOUNTED DRILL RIG USING 3-1/4 INCH I.D. HOLLOW-STEM AUGERS. DISTURBED SOIL SAMPLES WERE OBTAINED IN THE TEST BORINGS IN ACCORDANCE WITH THE STANDARD PENETRATION TEST (AASHTO T206) CONTINUOUSLY AND AT 2.5-FOOT TO 5.0-FOOT INTERVALS THROUGH THE SOIL USING AN AUTOMATIC HAMMER SYSTEM. THE HAMMER WAS CALIBRATED ON JULY 1, 2015 AND HAD A DRILL ROD ENERGY RATIO OF 81.9%.

CONTINUOUS SPLIT-SPOON SOIL SAMPLING WAS PERFORMED IN TEST BORING B-001-0-17 FOR A 7.5-FOOT INTERVAL BELOW THE APPROXIMATE STREAM BED ELEVATION. D50 VALUES WHICH HAVE BEEN CALCULATED FOR THE SCOUR ANALYSIS ARE PRESENTED ON THIS PAGE.

EXPLORATION FINDINGS

THE BORINGS EXHIBITED 6 TO 7 INCHES OF ASPHALT OVER 8 TO 9 INCHES OF BASE COURSE AT THE SURFACE

BELOW THE SURFACE COVER, THE BORINGS EXHIBITED COHESIVE SOILS DESCRIBED AS SANDY SILT (A-4a) OR SILT AND CLAY (A-6a) SOILS AND GRANULAR SOILS DESCRIBED AS GRAVEL AND/OR STONE FRAGMENTS WITH SAND AND SILT (A-2-4) EXTENDING DOWNWARDS TO A DEPTH OF 8.0 FEET.

BELOW THE NEAR SURFACE SOILS, THE BORINGS EXHIBITED BOTH GRANULAR AND COHESIVE SOILS DESCRIBED AS GRAVEL AND/OR STONE FRAGMENTS WITH SAND (A-1-b), COARSE AND FINE SAND (A-3a), SANDY SILT (A-4a) OR SILT AND CLAY (A-6a) SOILS EXTENDING DOWNWARDS TO THE DRILLED DEPTHS. THE COHESIVE A-4g AND A-6g SOILS ENCOUNTERED BELOW 17.5 FEET WITHIN THIS LAYER WERE FURTHER CLASSIFIED AS GLACIAL TILL

GROUND WATER WAS ENCOUNTERED DURING DRILLING AT DEPTHS RANGING FROM 17.0 TO 20.0 FEET (ELEVATIONS 698.3 FEET AND 696.8 FEET, RESPECTIVELY). UPON COMPLETION OF DRILLING, GROUNDWATER LEVELS WERE MEASURED AT DEPTHS RANGING FROM 7.8 TO 17.4 FEET (ELEVATIONS 707.5 FEET AND 699.4 FEET, RESPECTIVELY).

SPECIFICATIONS

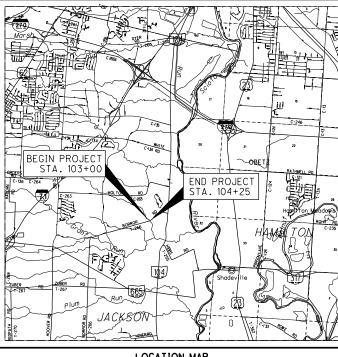
THIS GEOTECHNICAL EXPLORATION WAS PERFORMED IN ACCORDANCE WITH THE STATE OF OHIO, DEPARTMENT OF TRANSPORTATION, OFFICE OF GEOTECHNICAL ENGINEERING. SPECIFICATIONS FOR GEOTECHNICAL EXPLORATIONS, DATED JULY 2016.

AVAILABLE INFORMATION

ALL AVAILABLE SOIL INFORMATION THAT CAN BE CONVENIENTLY SHOWN ON THE SOIL PROFILE SHEETS HAS BEEN SO REPORTED. ADDITIONAL SUBSURFACE EXPLORATIONS MAY HAVE BEEN MADE TO STUDY SOME SPECIAL ASPECT OF THE PROJECT. COPIES OF THIS DATA, IF ANY, MAY BE INSPECTED IN THE FRANKLIN COUNTY ENGINEERS OFFICE.

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<u>LE</u>	EGEND	ODOT	CLASS	SIFIED	
	DESCRIPTION	CLASS	MECH./	'VISUAL	
6 6 6 8	GRAVEL AND/OR STONE FRAGMENTS WITH SAND	A-1-b	1	4	
	GRAVEL AND/OR STONE FRAGMENTS W/SAND AND SILT	A-2-4	1	0	
	COARSE AND FINE SAND	A-3a	2	8	
	SANDY SILT	A-4a	4	9	
	SILT AND CLAY	A-6a	2	5	
		TOTAL	10	26	
(XXXXX)	PAVEMENT OR BASE = X = APPROXIMATE THICKNESS	VISUAL			
	BORING LOCATION - PLAN VIEW.				
WC	INDICATES WATER CONTENT IN PERCENT.				
N ₆₀	INDICATES STANDARD PENETRATION RESISTANCE NORMALIZED TO 60% DRILL ROD ENERGY RATIO.				
W	INDICATES FREE WATER ELEVATION.				
0	INDICATES A NON-PLASTIC MATERIAL WITH A MOISTURE GREATER THAN 25 % OR GREATER THAN 19 % WITH A WE		NCE.		
SS	INDICATES A SPLIT SPOON SAMPLE.				
NP	INDICATES A NON-PLASTIC SAMPLE.				

		D ₅₀ LUES	
BORING NO.	SAMPLE NO.	ELEVATION	D ₅₀ VALUE
B-001-0-16	SS-5 SS-6 SS-7	705.8' - 704.3' 704.3' - 702.8' 702.8' - 701.3'	0.047 mm 0.046 mm 0.127 mm
B-002-0-16	SS-6	701.8′ - 700.3′	0.176 mm



LOCATION MAP





PARTICLE SIZE DEFINITIONS

12	2" 3	" 2.0	mm	0.42	? mm	0.07	4 mm	0.00	5 mm
BOULDERS	COBBLES	GRAVEL	COARSE	SAND	FINE	SAND	SIL	Т	CLAY
'		No. 10	SIEVE	No. 40	SIEVE	No. 200	SIEVE	· '	

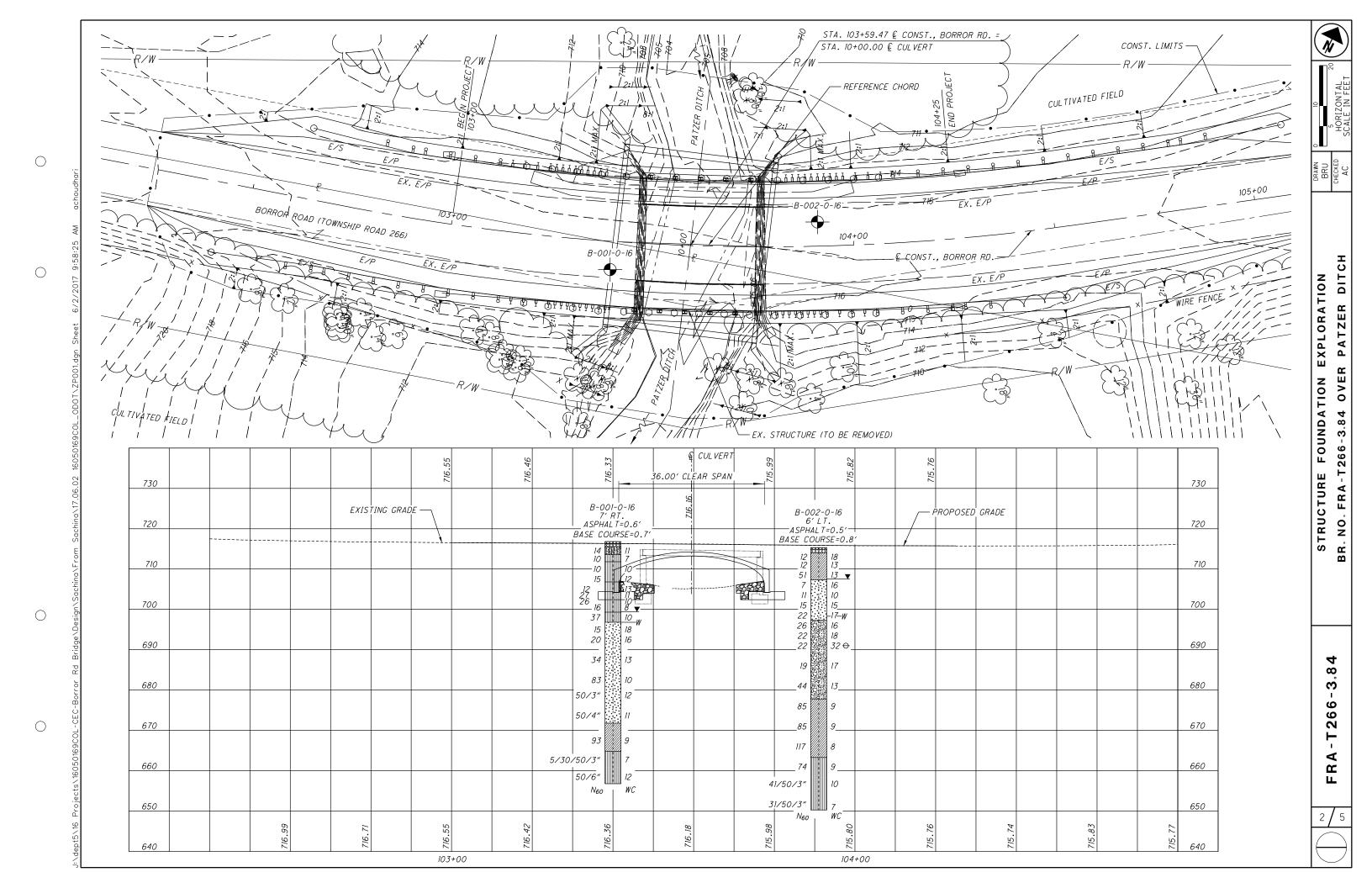
RECON. - LH 12/19/2016

DRILLING - CTL ENGINEERING, INC. 12/19/2016 - 12/20/2016

DRAWN - BRU 05/31/17 **REVIEWED -** JG 05/31/17







	FRA-T266-3.84 TRUCTURE FOUNDATION	DRILLING FIRM / OPE SAMPLING FIRM / LO	GGER:	CTL / JW	HAN	MER:	МО	OBILE B-5	ITAMC	C	STAT ALIG	NME	NT: _						EXPLOR B-001	
PID: START:12	SFN: 2531593 2/20/16 END: 12/20/16	DRILLING METHOD: _ SAMPLING METHOD:		.25" HSA SPT		IBRATI RGY F			7/1/15 81.9	_	COO							60 095.04	0.0 ft. 12 E	10
	MATERIAL DESCRII AND NOTES	PTION	ELEV. 716.8	DEPTHS	SPT/ RQD		REC (%)	SAMPLE ID	HP (tsf)		GRAI cs	DATIO	ON (%		AT LL	TERB PL	ERG PI	wc	ODOT CLASS (GI)	BA FI
Asphalt (7")			716.2	-	-		(70)	ID.	(toi)	OIX	00	10	01	OL				WO	, ,	T
Base course	: (8") Ense, dark brown, grave	EL AND/OR STONE	715.5	1	_															
FRAGMENT DAMP	S WITH SAND AND SILT, TR	ACE CLAY, FILL,	715.5 715.5 713.5	_ 2	9 7	14	44	SS-1	4.00	31	20	22	17	10	24	17	7	11	A-2-4 (0)	
	WN, SANDY SILT , LITTLE CL S, FILL, DAMP	AY, STONE		- 3 - 4	3 4	10	33	SS-2	-	-	-	-	-	-	-	-	-	7	A-4a (V)	
	F, BROWN, SANDY SILT , SON OSSIBLE FILL, MOIST	ME CLAY, TRACE	711.8	- 5 - 6	- 4	3														
@0 E!. LIADI	D. CONTAINS STONE FRACA			- 7 - 8	4 3	10	78	SS-3	4.00	-	-	-	-	-	-	-	-	10	A-4a (V)	
	D, CONTAINS STONE FRAGN		706.8	- 9 - 10	5	15	72	SS-4	4.50	-	-	-	-	-	-	-	-	12	A-4a (V)	
GRAVEL, M		AT, ETTILE		- - 11 - 12	3 3	12	83	SS-5	4.50	11	10	22	34	23	26	16	10	13	A-4a (4)	
@12.5'; TRA	ACE GRAVEL			— 13	6	27	78	SS-6	4.50	9	12	21	35	23	24	15	9	11	A-4a (5)	
@14.0'; SOM	ME GRAVEL, LITTLE CLAY			- 14 - - 15	4 6	26	83	SS-7	4.50	28	11	16	27	18	21	13	8	10	A-4a (2)	
			699.3	— 16 — 17	° 7	16	50	SS-8	4.50	-	-	-	-	-	-	-	-	8	A-4a (V)	
HARD, GRA TILL, DAMP	Y, SANDY SILT , LITTLE CLAY	Y AND GRAVEL,	696.8	18	8 12	37	100	SS-9	4.50	17	10	19	36	18	21	14	7	10	A-4a (4)	
	ENSE, BROWN, COARSE AND	D FINE SAND	696.8	W 20	15	5														-
SUIVIE GRA	VEL, LITTLE SILT, TRACE CL	AI, VVEI	<u> </u>	— 21 — 22	H ⁴ 5	15	89	SS-10	-	-	-	-	-	-	-	-	-	18	A-3a (V)	
				— 23 — 24	6	20	100	SS-11										16	A 20 (V)	
				- - 25	; = 9		100	55-11	-	_	-	-	-	-	-	-	-	16	A-3a (V)	
				- 26 - 27 - 27	-															
@28.5'; DEN	NSE, GRAY, MOIST			— 28 - — 29		34	100	SS-12	_	_	_	_	_		_	_	_	13	A-3a (V)	
				30	15			00 .2											7100(1)	
				- 32	! -															
@33.5'; VEF	RY DENSE, DAMP			33	25	83	94	SS-13	-	25	16	36	14	9	NP	NP	NP	10	A-3a (0)	
				— 35 — 36	-	9														
				- 37 - 38	-															
@38.5'; CON	NTAINS COBBLES, WET			39	50/3"	-	100	SS-14	-	_	-		-			-		12	A-3a (V)	
				- 40 - - 41	-															
				42	-															
@43.5'; TRA	ACE SILT, CLAY, DAMP		2	— 43 — — 44	50/4"	-	100	SS-15	-	-	-							11	A-3a (V)	-
HARD, GRA GRAVEL, TI	Y, SILT AND CLAY , SOME SALL, DAMP	AND, TRACE	671.8	- 45 - 46	-															
				47	· _															
				- 48 - - 49	9 25	93	89	SS-16	4.50	8	10	24	33	25	25	14	11	9	A-6a (5)	-
				- 50 - 51	-	3														1
HARD, GRA	Y, SANDY SILT , SOME CLAY AGMENTS, TILL, DAMP	, CONTAINS	664.8	- - 52 - - 53	-															
				— 53 — 54 —	5	-	100	SS-17	4.50	-	-	-	-	-	-	-	-	7	A-4a (V)	
				— 55 — 56	; -															
				- - 57 - 58	-															
			656.8	- 59 - 59	50	-	100	SS-18	4.00	-	-	-	-	-	-	-	-	12	A-4a (V)	1

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ŀ	ROJECT: FRA-T266-3.84 YPE: STRUCTURE FOUNDATION	DRILLING FIRM / OPERA SAMPLING FIRM / LOGG	ER:	CTL / L		_ HAM	IMER:	MOE	OBILE B-5 BILE AUTO	ITAMC	<u>C</u>	ALIG	NME	NT: _		:1					2-0-16
	ID: SFN:2531593 TART:12/19/16	DRILLING METHOD: SAMPLING METHOD:	3.	25" HSA SPT		_		ION DA RATIO (7/1/15 81.9	_	COO				3 (MS 9.586			65 134.72	5.0 ft. 245 E	PAGE 1 OF 2
	MATERIAL DESCRIPT AND NOTES	TON	ELEV. 715.3	DEPT	'HS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)		GRAI cs				ATT LL	PL	ERG PI	wc	ODOT CLASS (GI)	BACK FILL
-	Asphalt (6") Base course (9")		714.8		- - 1 -																
	/ERY STIFF, BROWN, SILT AND CLAY , SO FRACE GRAVEL, POSSIBLE FILL, DAMP	DME SAND,			- - 2 - - - 3 -	4 5 4	12	67	SS-1	2.50	8	11	22	35	24	33	19	14	18	A-6a (6)	
	@3.5'; STIFF, CONTAINS STONE FRAGME	NTS			- 4 - - 5 -	4 4 5	12	50	SS-2	2.00	-	-	-	-	-	-	-	-	13	A-6a (V)	
					- - 6 - - 7 -	3 4 33	51	56	SS-3	2.00	-	-	-	-	-	-	-	-	13	A-6a (V)	
	OOSE, BROWN, COARSE AND FINE SAN LITTLE GRAVEL, TRACE CLAY, MOIST		707.3	▼	- - - - - 9 -	1 2	7	67	SS-4	_	_	_		_	_	_	_	_	16	A-3a (V)	-
	@11.0'; MEDIUM DENSE				10 -	3															-
					- 12 - - - 13 -	3 5	11	50	SS-5	-	-	-	-	-	-	-	-	-	10	A-3a (V)	
					14 15	7 6 5	15	78	SS-6	-	11	20	38	22	9	NP	NP	NP	15	A-3a (0)	-
	@16.0'; WET		<u>69</u> 7.3	W	17 -	4 7 9	22	72	SS-7	-	-	-	-	-	-	-	-	-	17	A-3a (V)	-
	MEDIUM DENSE, BROWN, GRAVEL AND/ F RAGMENTS WITH SAND , LITTLE SILT, TR	OR STONE			- 18 - - - 19 - - - 20 -	4 9 10	26	94	SS-8	-	-	-	-	-	-	-	-	-	16	A-1-b (V)	-
		io (C) C io C io C, O Io			- - - 21 - - - 22 -	4 7 9	22	83	SS-9	-	-	-	-	-	-	-	_	-	18	A-1-b (V)	
					- - 23 - - - 24 -	5 6	22	100	SS-10		_	_	_	_	_	_	_	_	32	A-1-b (V)	-
					- - 25 - - - 26 -	10		100	30-10										- J2	A-1-0 (V)	-
					27 - 28 -																
					- 29 - - - 30 -	4 6 8	19	100	SS-11	-	31	28	19	17	5	NP	NP	NP	17	A-1-b (0)	-
					- 31 - - - 32 -																
	@33.5'; DENSE, TRACE CLAY				- 33 - - - 34 - -	9 13 19	44	100	SS-12	-	-	-	-	-	-	-	-	-	13	A-1-b (V)	
	@36.0'; HEAVY COBBLES		077.0		- 35 - - 36 - - 37 -																
	HARD, BROWNISH GRAY, SILT AND CLAY TRACE GRAVEL, CONTAINS COBBLES AN FRAGMENTS, TILL, DAMP		677.8		- - - - - - 39 -	24 26	85	78	SS-13	4.50	_	_		_			_	_	9	A-6a (V)	
					- - - - - 41 -	36		70		4.50										A-0a (V)	
					- - - - - - 43 -																
					- 44 - - 45 -	13 22 40	85	61	SS-14	4.50	-	-	-	-	-	-	-	-	9	A-6a (V)	_
					46 47	-															
					- 48 - - - 49 -	21 36 50	117	72	SS-15	4.50	-	-	-	-	-	-	-	-	8	A-6a (V)	
			663.3		50 51 52																
ı	HARD, GRAY, SANDY SILT , SOME CLAY, T CONTAINS COBBLES AND STONE FRAGM				- - 53 - - - 54 -	5 21	74	89	SS-16	4.50	_	_		_		_	_	_	9	A-4a (V)	
					- 55 - - 56 -	21 33			30-10	7.00										, ι πα (۷)	-
					- - - - - - 58 -	41															
	@58.5'; VERY STIFF, LITTLE CLAY				- 59 -	41 50/3"	-	89	SS-17	2.50	-	-	-	-	-	-	-	-	10	A-4a (V)	-

 \bigcirc

 \bigcirc \bigcirc \bigcirc

SFN: 103+91, 6' LT. PID: 2531593 PROJECT: FRA-T266-3.84 STATION / OFFSET: START: <u>12/19/16</u> END: 12/19/16 PG 2 OF 2 B-002-0-16 GRADATION (%)
GR CS FS SI CL MATERIAL DESCRIPTION ELEV. SPT/ RQD N₆₀ REC SAMPLE HP ATTERBERG BACK FILL DEPTHS AND NOTES (%) ID (tsf) 655.3 HARD, GRAY, **SANDY SILT**, SOME CLAY, TRACE GRAVEL, CONTAINS COBBLES AND STONE FRAGMENTS, TILL, DAMP 61 (continued) 62 63 @63.5'; HARD, SOME CLAY 64 A-4a (V) 4.50 SS-18

NOTES: CAVED AT 17.3'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: NOT RECORDED

APPENDIX B TEST BORING RECORDS



SOIL DESCRIPTION

Descriptors for soil consistency used in this report are based upon the Standard Penetration Test (SPT), ASTM D 1587, with the penetration (N) values corrected to N_{60} , based upon the efficiency of the SPT Hammer used for the soil sampling.

Descriptors for both non-cohesive and cohesive soils are presented below, with the corresponding range of corrected penetration values.

NON-COHESIVE SOIL CORRECTED PENETRATION VALUES **DESCRIPTION BLOWS PER FOOT (BPF)** Very Loose.....0 – 4 Very Dense......Over 50 **COHESIVE SOIL CORRECTED PENETRATION VALUES BLOWS PER FOOT (BPF) DESCRIPTION** Very Soft......0 – 1 Medium Stiff......5 – 8 Hard.....Over 30

SOIL DESCRIPTION	MOISTURE TERMS	DESCRIPTION
Powdery	Dry	Powderv
		Below Plastic Limit
Damp to the Touch	Moist	Above Plastic, Below Liquid Limit
Free Water	Wet	Above Liquid Limit
		•

COHESIVE SOIL

Moisture term descriptors for both non-cohesive and cohesive soils are presented below.

NON-COHESIVE



STATE 12/20/16 END 12/20/16 SAMPLING METHOD: SPT ENERGY FATTO (%): 81.9 COORD: 673175.6011 N. 181809-06.	TYPE: STRUCTURE FOUNDATION SA	RILLING FIRM / OPERATOR: _		HAMME	ER: MO	IOBILE B-5 BILE AUTO		<u> </u>	ALIGN	MEN ⁻						EXPLORA B-001	-0-16
Second Region Second Regio		· · · · · · · · · · · · · · · · · · ·	3.25" HSA									•				0 ft.	PAGE 1 OF 2
AND NOTES			1	CDT/	DEC			_							093.04	ODOT	BACK
Title Diagram Title Di			I DEPTHS I											_	wc	CLASS (GI)	FILL
### RAMENTS WITH SAND AND SILT, TRACE CLAY, FILL, DAMP STIFF BROWN, SANDY SILT, LITTLE CLAY, STONE FRAGMENTS, FILL, DAMP	Base course (8")	715.															
STIFF, BROWN, SANDY SILT, LITTLE CLAY, STONE FRAGMENTS, FILL, DAMP VERY STIFF, BROWN, SANDY SILT, SOME CLAY, TRACE GRAVEL, POSSIBLE FILL, MOIST 711.8 71.8	FRAGMENTS WITH SAND AND SILT, TRACE C	CLAY, FILL,		7 1	14 44	SS-1	4.00	31	20	22	17 10	24	17	7	11	A-2-4 (0)	
VERY STIFF, BROWN, SANDY SILT, SOME CLAY, TRACE GRAVEL, POSSIBLE FILL, MOIST		TONE	8	3 4 1	10 33	SS-2	-	-	-	-	- -	-	-	-	7	A-4a (V)	
@8.5'; HARD, CONTAINS STONE FRAGMENTS 706.8 HARD, BROWN, SANDY SILT, SOME CLAY, LITTLE @12.5'; TRACE GRAVEL @14.0'; SOME GRAVEL, LITTLE CLAY HARD, GRAY, SANDY SILT, LITTLE CLAY AND GRAVEL, TILL, DAMP @9.5 15 72 SS-4 4.50 12 10 10 10 11 3 6 12 83 SS-5 4.50 11 10 22 34 23 26 16 10 13 8 12 13 6 8 27 78 SS-6 4.50 9 12 13 5 6 83 SS-7 4.50 28 11 16 27 18 21 13 8 10 MEDIUM DENSE, BROWN, COARSE AND FINE SAND, SOME GRAVEL, LITTLE SILT, TRACE CLAY, WET 18 8 19 10 10 10 10 10 10 11 3 6 12 83 SS-5 4.50 11 10 22 34 23 26 16 10 13 11 13 8 10 11 11 12 14 12 15 16 17 18 18 18 19 11 18 19 11 18 18	VERY STIFF, BROWN, SANDY SILT , SOME CLA GRAVEL, POSSIBLE FILL, MOIST	AY, TRACE	- 6 -		10 78	SS-3	4.00	_	-	-		-	-	-	10	A-4a (V)	
HARD, BROWN, SANDY SILT, SOME CLAY, LITTLE GRAVEL, MOIST @12.5'; TRACE GRAVEL @14.0'; SOME GRAVEL, LITTLE CLAY HARD, GRAY, SANDY SILT, LITTLE CLAY AND GRAVEL, TILL, DAMP HARD, BROWN, SANDY SILT, LITTLE CLAY AND GRAVEL, TILL, DAMP MEDIUM DENSE, BROWN, COARSE AND FINE SAND, SOME GRAVEL, LITTLE SILT, TRACE CLAY, WET 10	@8.5'; HARD, CONTAINS STONE FRAGMENTS		- 9 -	7 5 1	15 72	SS-4	4.50	_	_	_		-	_	_	12	A-4a (V)	
HARD, GRAY, SANDY SILT, LITTLE CLAY AND GRAVEL, TILL, DAMP MEDIUM DENSE, BROWN, COARSE AND FINE SAND, SOME GRAVEL, LITTLE SILT, TRACE CLAY, WET - 16				6	1-											(7)	
HARD, GRAY, SANDY SILT, LITTLE CLAY AND GRAVEL, TILL, DAMP MEDIUM DENSE, BROWN, COARSE AND FINE SAND, SOME GRAVEL, LITTLE SILT, TRACE CLAY, WET - 16	@12.5'; TRACE GRAVEL		12	3 1 6												A-4a (4)	
HARD, GRAY, SANDY SILT, LITTLE CLAY AND GRAVEL, TILL, DAMP MEDIUM DENSE, BROWN, COARSE AND FINE SAND, SOME GRAVEL, LITTLE SILT, TRACE CLAY, WET - 16 - 3 5 7 16 50 SS-8 4.50 8 - 17 - 18 - 8 12 37 100 SS-9 4.50 17 10 19 36 18 21 14 7 10	@14.0'; SOME GRAVEL, LITTLE CLAY		14	12							_	+				A-4a (5) A-4a (2)	
HARD, GRAY, SANDY SILT, LITTLE CLAY AND GRAVEL, TILL, DAMP MEDIUM DENSE, BROWN, COARSE AND FINE SAND, SOME GRAVEL, LITTLE SILT, TRACE CLAY, WET			16	3 5 _ 1	16 50	SS-8			-	-		-	-	-		A-4a (V)	_
MEDIUM DENSE, BROWN, COARSE AND FINE SAND , SOME GRAVEL, LITTLE SILT, TRACE CLAY, WET - 21			3 10 -	8	27 400	00.0	4.50	47	40	40	00 40	0.4	14	_	40	A 4- (4)	
SOME GRAVEL, LITTLE SILT, TRACE CLAY, WET -21 -35 -36 -36 -37 -38 -38 -38 -38 -38 -38 -38	MEDIUM DENSE BROWN COARSE AND FINE		8 W - 1		37 100	55-9	4.50	17	10	19 .	36 18	3 21	14	/	10	A-4a (4)	
- 23				5 1	15 89	SS-10	-	-	-	-		-	-	-	18	A-3a (V)	-
25 9 20 100 55-11 16				6	20 400	00.11									16	A 20 () ()	
			- 25 - - 26 -		20 100	55-11	-	_	-	-	- -	-	-	-	10	A-3a (V)	
@28.5'; DENSE, GRAY, MOIST	@28.5'; DENSE, GRAY, MOIST		- 28 -		24 465	00.46									10	A-3a (V)	

MEDIUM DENSE, BROWN COARSE AND FINE SAND. 868 870 870 870 870 870 870 870	PID:	SFN:	2531593	PROJECT:	FRA-T2	266-3.84		STATION	OFFSE			10, 7' RT.		TART:	12/2	20/16	EN	ID: _	12/2	0/16	_ P	G 2 OI	2 B-00	1-0-16
MEDIUM DENSE, BROWN, COARSE AND FINE SAND, SOME GRAVEL, LITTLE SILT, TRACE CIAY, WET (continued) 888.8		MAT	ERIAL DESCRIP	TION		ELEV.	DE	DTUC	SPT/	N		SAMPLE	HP	(GRAD.	ATIO	N (%)		ATT	ERBE	RG		ODOT	BACK
MEDIUN DENSE, BROWN COARSE AND FINE SAND. 33 - 33 - 33 - 33 - 33 - 33 - 34 - 25 - 16 - 36 - 14 - 9 - NP - NP - NP - 10 - A-3a (V) - 32 - 33 - 34 - 25 - 33 - 35 - 36 - 37 - 38 - 36 - 37 - 38 - 36 - 37 - 38 - 36 - 37 - 38 - 36 - 37 - 38 - 36 - 37 - 38 - 37 - 38 - 38 - 37 - 38 - 38			AND NOTES			686.8		PINS	RQD	IN ₆₀	(%)	ID	(tsf)	GR	CS	FS	SI	CL	LL	PL	PI	WC	CLASS (GI)	FILL
@38.5; CONTAINS COBBLES, WET 30	SOME GRAVEI	_, LITTLE S	IILT, TRACE CLA	FINE SAND, AY, WET (continued)				- - - - - - 33 -	25															
@43.5; TRACE SILT, CLAY, DAMP HARD, GRAY, SILT AND CLAY, SOME SAND, TRACE GRAVEL, TILL, DAMP HARD, GRAY, SANDY SILT, SOME CLAY, CONTAINS STONE FRAGMENTS, TILL, DAMP 664.8 664.8 665.8 665.8 665.8 666.8 671.8								- - - - - - - - - - - 36 - - - - - - - - - -	32 29				-											
HARD, GRAY, SILT AND CLAY, SOME SAND, TRACE GRAVEL, TILL, DAMP 671.8 6	@38.5'; CONTA	AINS COBB	LES, WET					- - - - - - - - - 41 - - - - - - - -								-					_			
HARD, GRAY, SANDY SILT, SOME CLAY, CONTAINS STONE FRAGMENTS, TILL, DAMP 664.8 -51 -52 -53 -54 -58 -59 -50 -51 -52 -53 -54 -55 -56 -57 -58 -59 -50 -50 -51 -50 -51 -52 -53 -54 -55 -55 -56 -57 -58 -59 -50 -50 -50 -50 -50 -50 -50	HARD, GRAY,	SILT AND		ND, TRACE		<u>671.8</u>		- 45 - - 46 - - 47 - - 48 -			_100,	SS-15		-	_	-	-	-	-	-	-	11	A-3a (V)	
- 55 55 56 57 58 59 50 - 100 SS-18 4.00 12 A-4a (V)	HARD, GRAY, STONE FRAGM	SANDY SIL MENTS, TIL	.T, SOME CLAY, L, DAMP	CONTAINS		_664.8_		- 50 - 51 - 52 -	25	93	89	SS-16	4.50	8	10	24	33	25	25	14	11	9	A-6a (5)	
656.8 100 SS-18 4.00 12 A-4a (V)								- 55 - 56 - 57 -	50/3"	-	100	SS-17	4.50	-	-	-	-	-	-	-	-	7	A-4a (V)	
						656.8	EOB	<u>-</u> 59 -	50	-	100	SS-18	4.00	-	-	-	-	-	-	-	-	12	A-4a (V)	

PROJECT:	: FRA-T266-3.84 STRUCTURE FOUNDATION	_ DRILLING FIRM / OPER SAMPLING FIRM / LOGO		CTL / LH CTL / LH	-			OBILE B-5			STATION / OFFSET: 103+91, 6' LT. ALIGNMENT:							LT.	EXPLORATION ID B-002-0-16	
PID:	SFN: 2531593	DRILLING METHOD:	· · · · · · · · · · · · · · · · · · ·			HAMMER: MOBILE AUTOMATIC CALIBRATION DATE: 7/1/15					ELEVATION: 715.3 (MSL) EOB:						6	PAGE		
	START: 12/19/16 END: 12/19/16 SAMPLING METHO			SPT		ENERGY RATIO (%): 81.9			COORD: 673209.5864 N, 181813								1 OF 3			
	MATERIAL DESCRI	 PTION	ELEV.	DEDTUG	SPT/			SAMPLE	HP		GRAD	DATIC					ERG		ODOT	BACK
	AND NOTES		715.3	DEPTHS	RQD		(%)	ID		GR	CS	FS	Sì	CL		_		wc	CLASS (GI)	FILL
_ Asphalt (6	6")		714.8																	
Base cour	· /		714.0	<u></u>	-															
VERY ST TRACE G	TIFF, BROWN, SILT AND CLAY , BRAVEL, POSSIBLE FILL, DAMP	SOME SAND,		_ 2 _ _ 3 _	4 5 4	12	67	SS-1	2.50	8	11	22	35	24	33	19	14	18	A-6a (6)	
@3.5'; ST	TIFF, CONTAINS STONE FRAGM	IENTS		- 4 -	4 4 5	12	50	SS-2	2.00	-	-	-	-	-	-	-	-	13	A-6a (V)	-
				- 5 - - 6 - - 7	3	51	56	00.2	2.00									40	A C = 0.0	
10085 1	BROWN, COARSE AND FINE SA	ND COME SILT	707.3	▼ - 7 -	33		50	SS-3	2.00	-	-	-	-	-	-	-	-	13	A-6a (V)	_
	BROWN, COARSE AND FINE SA BRAVEL, TRACE CLAY, MOIST	ND, SOME SILT,		9 -	1 2 3	7	67	SS-4	-	-	-	-	-	-	-	-	-	16	A-3a (V)	
@11.0'; M	@11.0'; MEDIUM DENSE @16.0'; WET				3															
				- 12 - - 13 -	3 5	11	50	SS-5	-	-	-	-	-	-	-	-	-	10	A-3a (V)	-
				- 14 -	7 6 5	15	78	SS-6	-	11	20	38	22	9	NP	NP	NP	15	A-3a (0)	_
@16.0'; V					4 _															
- 			697.3	W	7 9	22	72	SS-7	-	-	-	-	-	-	-	-	-	17	A-3a (V)	_
	DENSE, BROWN, GRAVEL AND : NTS WITH SAND, LITTLE SILT,		d D	19	4 9 10	26	94	SS-8	-	-	-	-	-	-	-	-	-	16	A-1-b (V)	-
				- 20 - - - 21 -	4															
			T S	_ 22 -	7 9	22	83	SS-9	-	-	-	-	-	-	-	-	-	18	A-1-b (V)	-
			7 2 4 0	- 23 - - 24 - - 25 -	5 6 10	22	100	SS-10	-	-	-	-	-	-	-	-	-	32	A-1-b (V)	_
				26																
		à Q à Q 0 (- 27 - - 28 -																
			D T	29 -	4 6 8	19	100	SS-11	-	31	28	19	17	5	NP	NP	NP	17	A-1-b (0)	

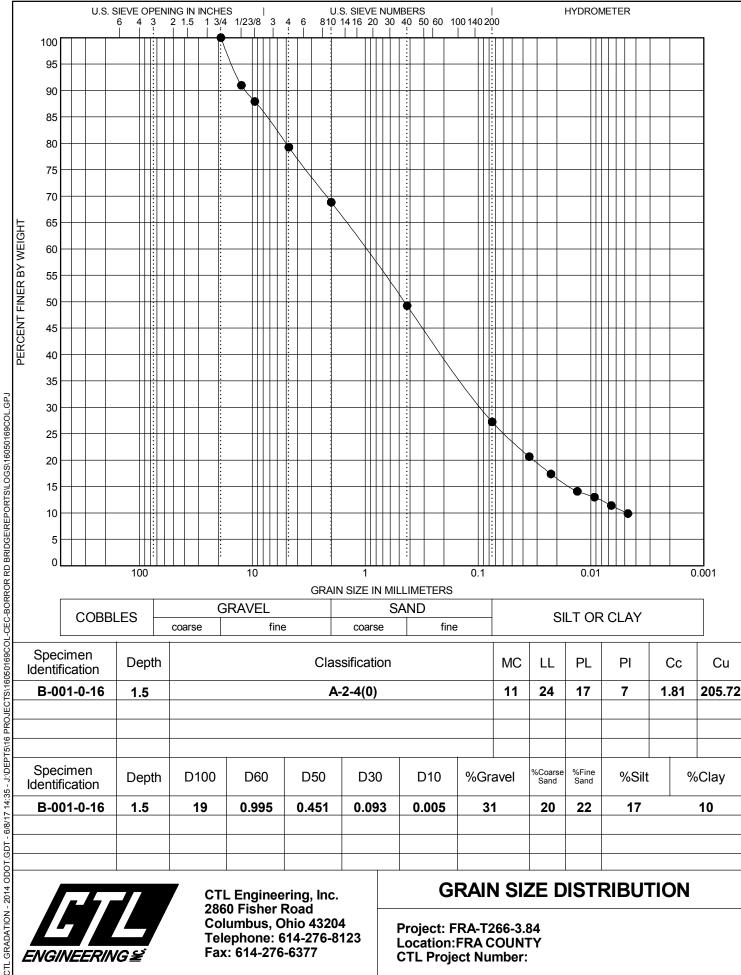
PID:	SFN:	2531593	PROJECT:	FRA-T	266-3.84						TART	: 12/	19/16	EN	ND: _	12/19/16		_ P	G 2 O	F 3 B-00)2-0-16	
	MAT	ERIAL DESCRIP	PTION		ELEV.	DEPTHS	SPT/	N ₆₀		SAMPLE			GRAD					ERBI			ODOT CLASS (CI)	BACK
MEDILINA DENIC	OF PROM	AND NOTES	(OD OTONE	R•V•	685.3	726	RQD	60	(%)	ID	(tsf)	GR	cs	FS	SI	CL	LL	PL	PI	WC	CLASS (GI)	FILL
		N, GRAVEL AND . D , LITTLE SILT, T	race Clay, Wet			- - - - - - - - - - - - - - - - - - -	- - - -															
@33.5'; DENSE	E, TRACE C	CLAY				33 - 34 - 35 -	9 13 19	44	100	SS-12	-	-	-	-	-	-	-	-	-	13	A-1-b (V)	
			N, LITTLE SAND,		677.8	- 36 - - 37 -	_ _ _															
TRACE GRAVE FRAGMENTS,	EL, CONTAI	INS COBBLES A	ND STONE			38 - 39 - 40 -	24 26 36	85	78	SS-13	4.50	-	-	-	-	-	-	-	-	9	A-6a (V)	
HARD, BROWN TRACE GRAVE FRAGMENTS,						41 42 43	- - - -															
							13 22 40	85	61	SS-14	4.50	-	-	-	-	-	-	-	-	9	A-6a (V)	
						46 - 47 - 48 - 49 -	21	117	72	SS-15	4.50									8	A-6a (V)	
HARD, GRAY,	CANDY SIL	T SOME CLAY	TRACE GRAVEL,		663.3	- 50 - 51 - 52 -	50		12	33-13	4.30	-	-	-	-	-	-	-	-	0	A-0a (V)	
CONTAINS CO	BBLES AN	IT, SOME CLAT, ID STONE FRAG	MENTS, TILL, DAN	1 P		- 53 - - 54 - - 55 -	5 21 33	74	89	SS-16	4.50	-	-	-	-	-	-	-	-	9	A-4a (V)	
						- 56 - - 56 - - 57 - - 58 -	- - - -															
@58.5'; VERY \$	STIFF, LITT	TLE CLAY				- 59 - - 60 -	41 50/3"	-	89	SS-17	2.50	-	-	-	-	-	-	-	-	10	A-4a (V)	
STANDARD ODOL SOIL BORING LOG (8:5 x 1j) @28.2; VERY STANDARD ODOL SOIL BORING LOG (8:5 x 1j)	STIFF, LITI	TLE CLAY				- 55 - 56 - 57 - 58 - 59 -	33						-			-		-				

D:	_ SFN: _	2531593	PROJECT:	FRA-T	266-3.84	S	TATION /	OFFSE	T:	103+9	1, 6' LT.	_ S1	TART	12/1	9/16	EN	N D: _	12/1	9/16_	PG 3	3 OF	3 B-00	2-0-1
		TERIAL DESCRIP	TION		ELEV.	DED	TLIC	SPT/		REC	SAMPLE	HP	(SRAD/	ATIO	N (%)	ATT	ERBER	G 📗		ODOT	BAC
		AND NOTES			653.1	DEP ⁻	IH5	RQD	N ₆₀	(%)	ID	(tsf)	GR	CS	FS	SI	CL	LL	PL F	ı v	vc '	CLASS (GI)	FIL
CONTAINS C	(, SANDY S COBBLES A	ILT , SOME CLAY, ND STONE FRAGI	TRACE GRAVEL MENTS, TILL, DA	_, AMP			- - 63 -																
continued) 1063.5'; HAR	D, SOME C	LAY			650.3		F 7	31 _50/3"_	-	100	SS-18	4.50	-	-	-	-	-	-	-		7	A-4a (V)	
						EOB-	65																

ABANDONMENT METHODS, MATERIALS, QUANTITIES: NOT RECORDED

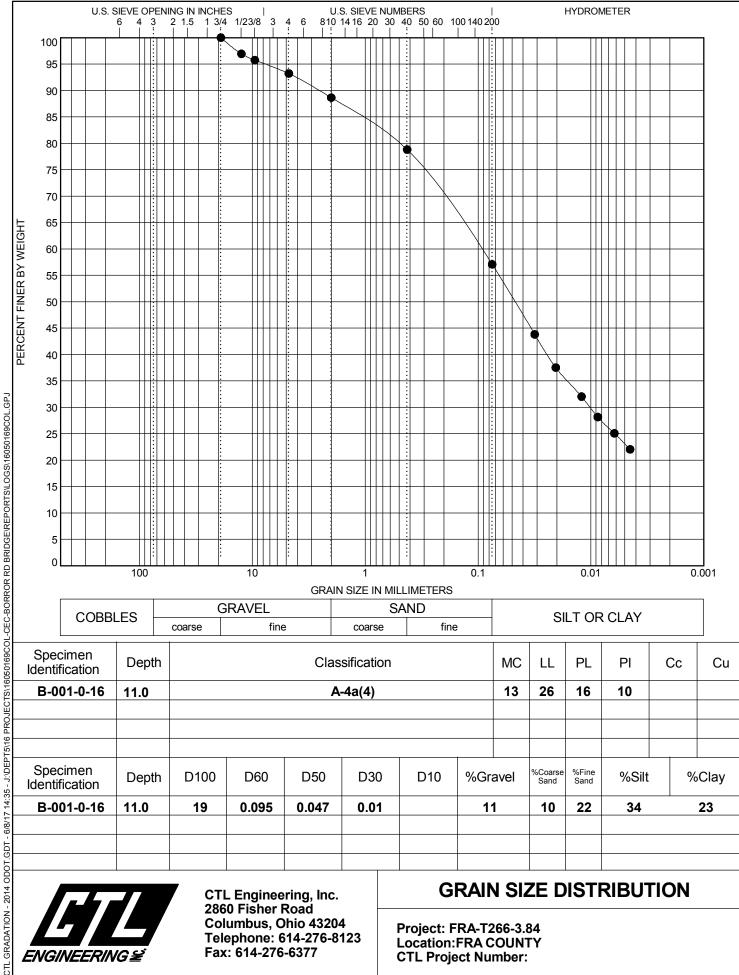
APPENDIX C LABORATORY TEST SHEETS



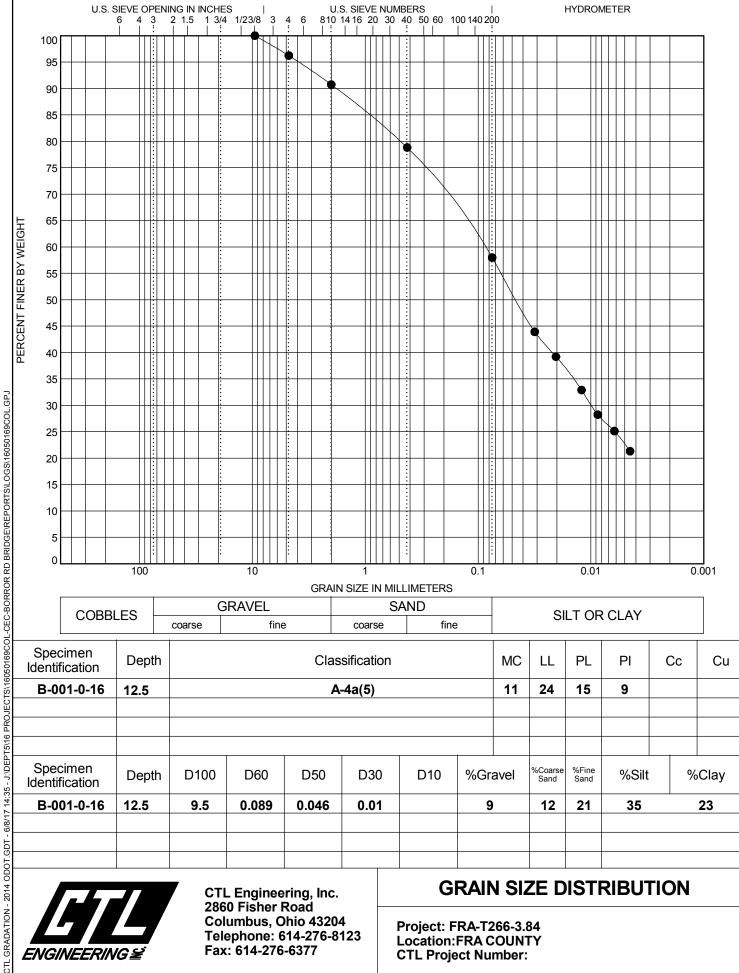




GRAIN SIZE DISTRIBUTION

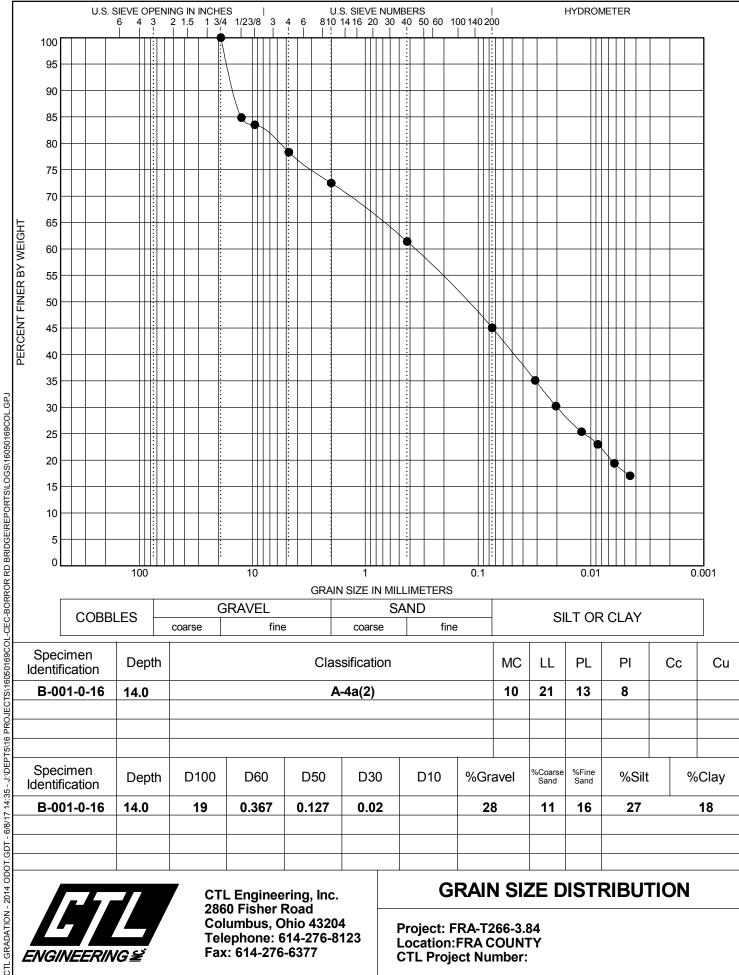




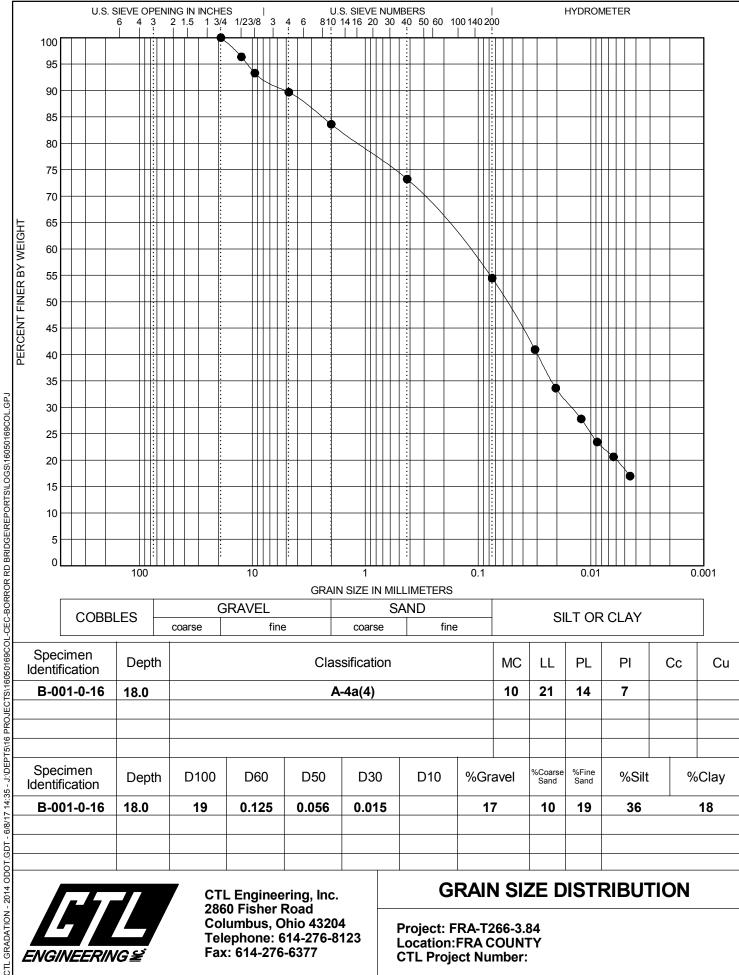




GRAIN SIZE DISTRIBUTION

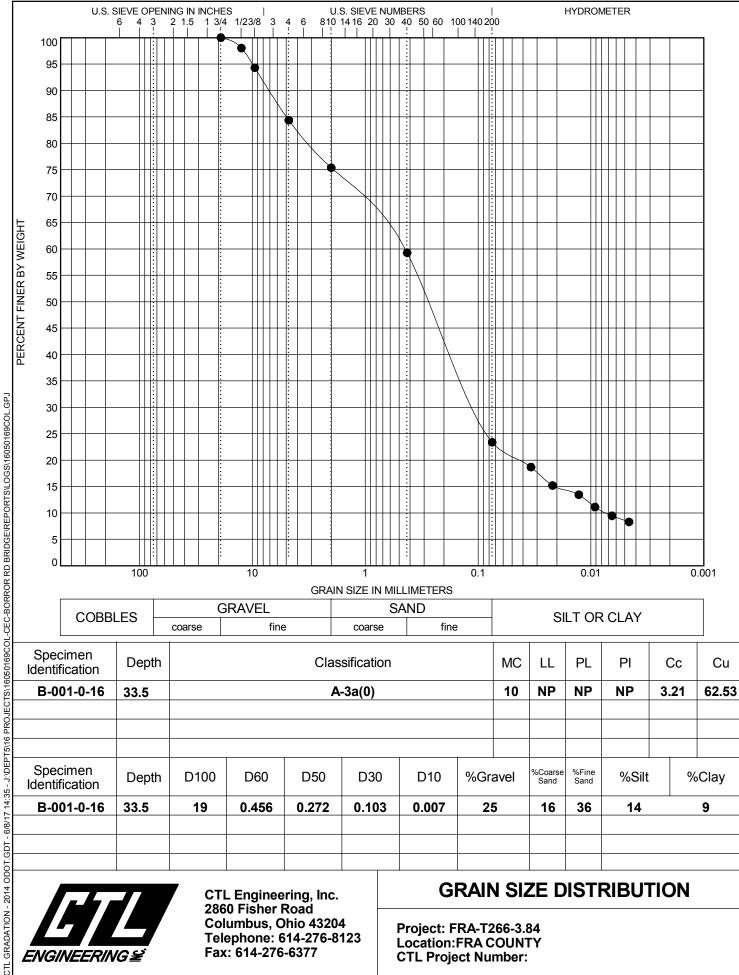






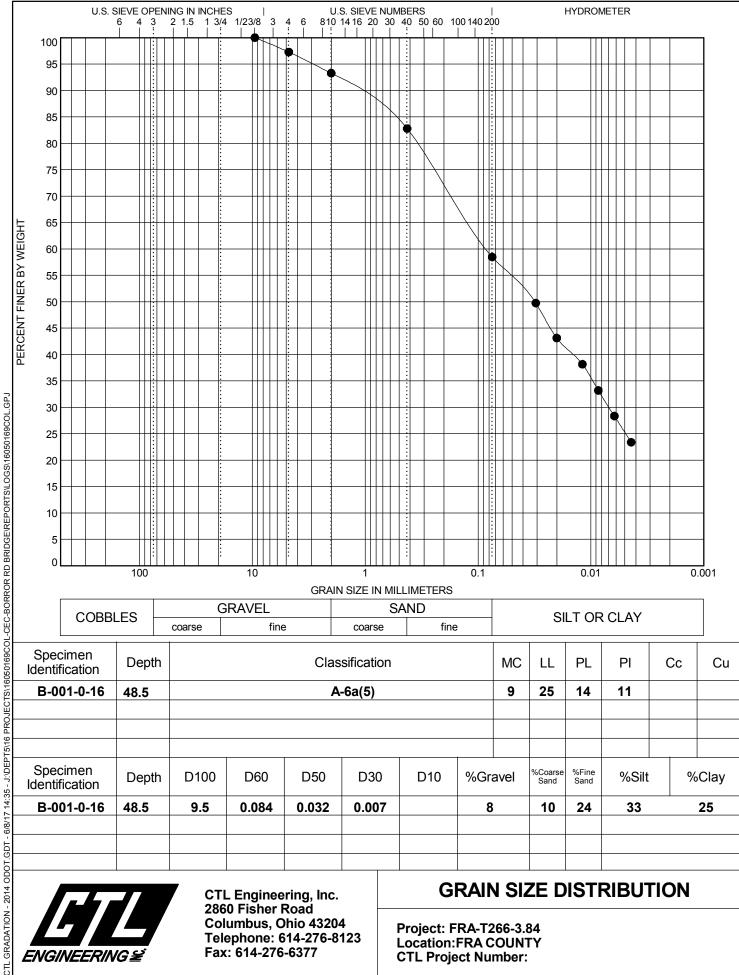


GRAIN SIZE DISTRIBUTION



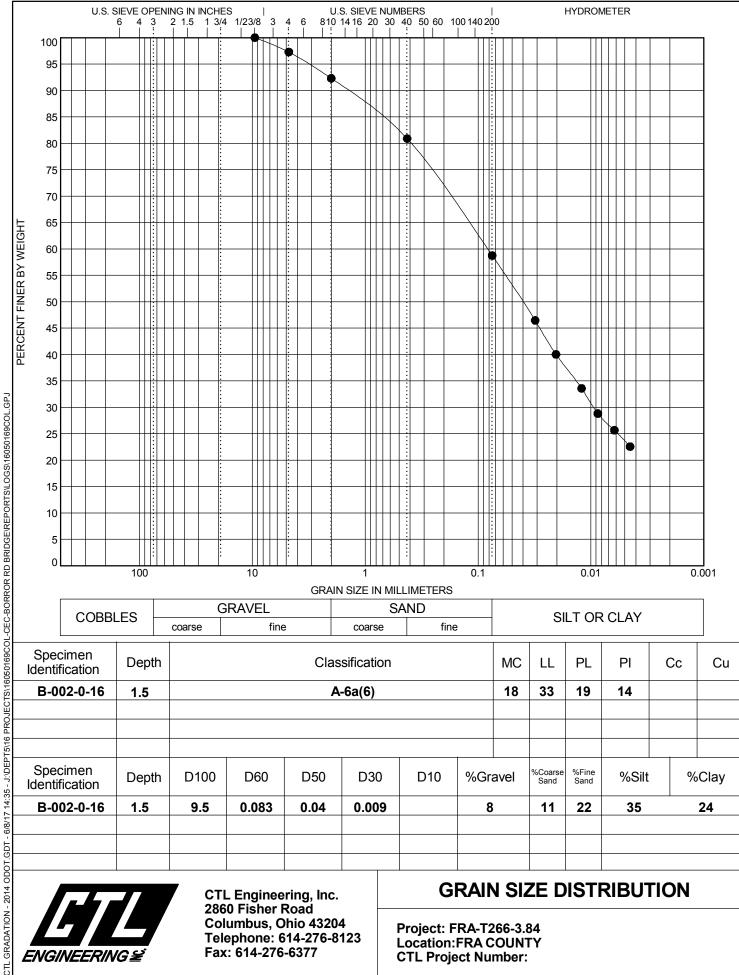


2860 Fisher Road Columbus, Ohio 43204 Telephone: 614-276-8123 Fax: 614-276-6377



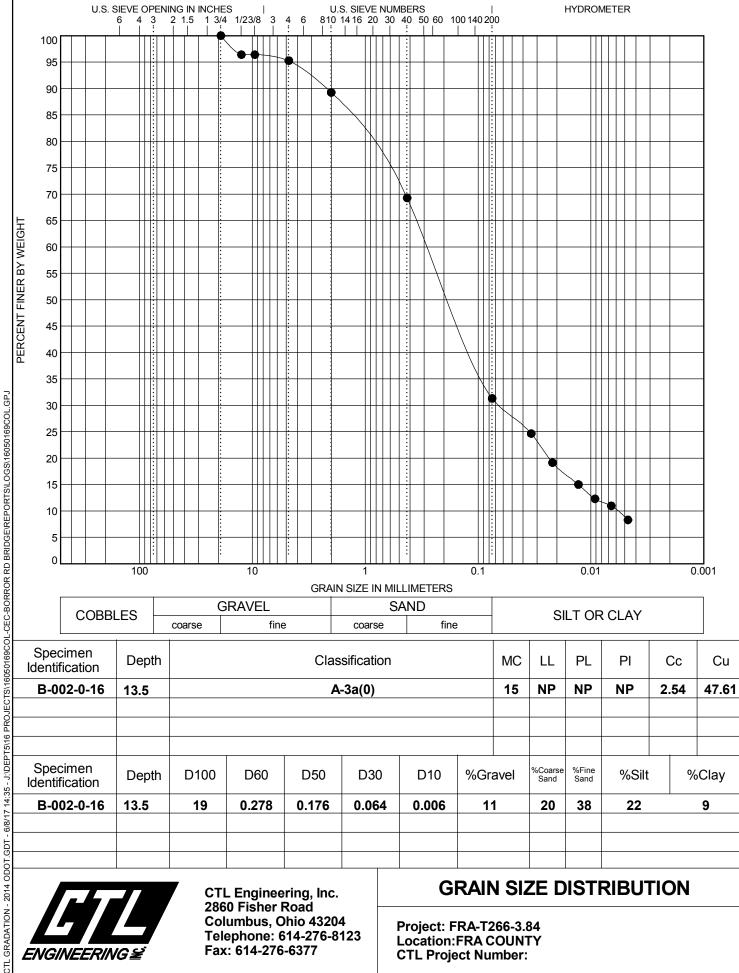


GRAIN SIZE DISTRIBUTION



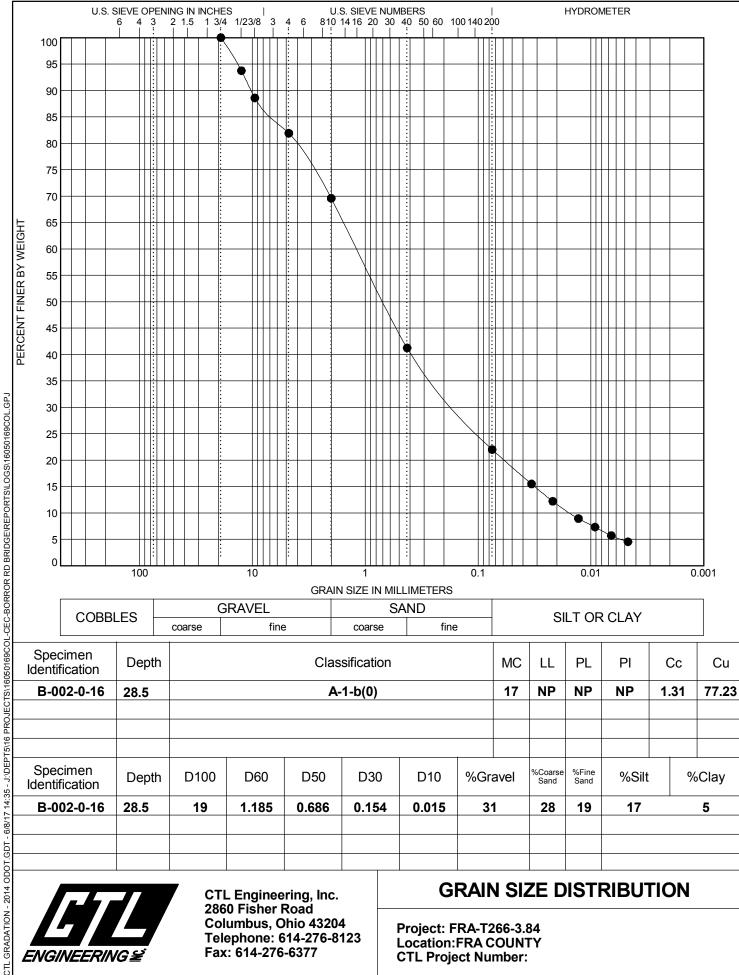


GRAIN SIZE DISTRIBUTION





2860 Fisher Road Columbus, Ohio 43204 Telephone: 614-276-8123 Fax: 614-276-6377





APPENDIX D BEARING RESISTANCE CALCULATIONS



Project Borror Road Bridge over Patzer Ditch

 Project No.
 16050169COL

 Boring No.
 B-001-0-16

Bearing Resistance- Strength Limit State

Cohesion, c	3.0	ksf
Friction Angle, ϕ_b	0	Degrees
Footing Width, B	9.00	feet
Unit Wt. of Soil, Y	0.125	kcf
Footing Length, L _f	35	ft
Footing Embedment Depth, D _f	4.5	ft
GW Depth Below Footing, D _W	0	ft

Nom. Bearing Resistance, q _n	16.5 ksf	$= c_f N_c s_c + \gamma D_f N_q s_q d_q C_{Wq} + 0.5 \gamma B N_\gamma s_\gamma C_{W\gamma}$
Where N _c	5.14	
	3.14	T-bl- 40 0 0 4 0- 4
N_q	ı	Table 10.6.3.1.2a-1
N_{γ}	0	
S _c	1.05	$=1+(B/L_f)^*(N_q/N_c)$; or $1+(B/5Lf)$ for $\phi = 0$
S_q	1.00	=1+(B/L _f)*tan ϕ_f ; or 1.0 for ϕ = 0 Table 10.6.3.1.2a-3
s_γ	1.00	=1-0.4*(B/L _f); or 1.0 for $\phi = 0$
C_{Wq}	0.50	Table 10.6.3.1.2a-2
$C_{W\gamma}$	0.50	
1.5B+D _f	18.00 ft	For Cw Check
D_f/B	0.50	For dq by Hansen 1970
d_q	1.00	Hansen 1970 or Table 10.6.3.1.2a-4

Fact. Bearing Resistance, q_r 8.2 ksf = $\phi_b^* q_n$

Resistance Factor, ϕ_b 0.5 Table 10.5.5.2.2-1

Bearing Resistance- Service Limit State

Pres. Bearing Resistance, qr	8.0 ksf	Table C10.6.2.6.1-1
Resistance Factor, φ _r	1.0	Section 11.5.7

Project Borror Road Bridge over Patzer Ditch

Project No. 16050169COL **Boring No.** B-002-0-16

Bearing Resistance- Strength Limit State

Cohesion, c	0.0	ksf
Friction Angle, ϕ_b	30	Degrees
Footing Width, B	9.00	feet
Unit Wt. of Soil, Y	0.125	kcf
Footing Length, L _f	35	ft
Footing Embedment Depth, Df	4.5	ft
GW Depth Below Footing, Dw	0	ft
Nom Posting Posistance a	10 5	kof

Nom. Bearing Resistance, q _n	12.5 kst	$= C_f N_c s_c + \gamma D_f N_q s_q d_q C_{Wq} + 0.5 \gamma B N_\gamma s_\gamma C_{W\gamma}$

Where

30.1 N_c N_q 18.4

22.4 N_{γ}

 \mathbf{S}_{C} $=1+(B/L_f)^*(N_q/N_c)$; or 1+(B/5Lf) for $\phi = 0$ 1.16

 $=1+(B/L_f)*tan\phi_f$; or 1.0 for $\phi=0$ 1.15 Table 10.6.3.1.2a-3 \mathbf{S}_{q}

Table 10.6.3.1.2a-1

For Cw Check

0.90 =1-0.4*(B/L_f); or 1.0 for $\phi = 0$ S_{γ}

 C_{Wq} 0.50 Table 10.6.3.1.2a-2

 $C_{W\gamma}$ 0.50 1.5B+D_f 18.00 ft

 D_f/B 0.50 For dq by Hansen 1970

Hansen 1970 or Table 10.6.3.1.2a-4 d_{q} 1.14

Fact. Bearing Resistance, q_r 5.6 ksf $=\phi_b^*q_n$

Resistance Factor, ϕ_b 0.45 Table 10.5.5.2.2-1

Bearing Resistance- Service Limit State

Pres. Bearing Resistance, qr 5.0 ksf Table C10.6.2.6.1-1

Resistance Factor, ϕ_r 1.0 11.5.7